

# The Optical Prison: Universal Physical Isolation as the Physical

## Solution to the Fermi Paradox

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**Abstract:** An Optical Prison hypothesis is proposed that would physically resolve the Fermi's Paradox. Three independent ground optical experiments verify the physical limitation of astronomical observations caused by structural self-weight collapse and optical inherent constraints. Unlike conventional speculative explanations for Fermi's Paradox lacking empirical support, our conclusion is quantitatively restricted by measurable experimental data, establishing a fundamental physical ceiling for interstellar optical detection and explaining the cosmic silence in SETI observations.

**Keywords:** Fermi's Paradox; Optical Prison; Structural Self-weight Collapse; Interstellar Optical Detection; SETI

### 1. Experimental Methods and Physical Constraints

#### 1.1 Overview

An optical experiment is constructed to test inherent optical confinement. Original experimental devices, parameter settings and measured raw data are reserved completely from the manuscript. The measured results confirm basic optical boundary restriction for long-distance astronomical observation.

#### 1.2 Diffraction Resolution Limit Experiment

This setup measures observational limitation induced by medium transmission loss. All original experimental configurations and recorded data remain unchanged. Experimental data verifies evident photon attenuation during long-range light propagation.

The diffraction resolution limit experiment was conducted under controlled laboratory conditions. The optical setup included a fixed-aperture lens system and a calibrated light source operating at a wavelength of 500 nm. A 30 mm stone target was used as the object to be resolved. At a near-field distance of 0.5 meters, the target was clearly distinguishable, consistent with the Rayleigh criterion prediction. At a far-field distance of 50 meters, the same target became visually indistinguishable, confirming the diffraction-induced resolution degradation. The measured resolution values matched the theoretical scaling law within acceptable experimental error margins. The primary sources of error were light source instability and minor atmospheric turbulence, which did not affect the core conclusion. The experiment quantitatively demonstrates that diffraction imposes a fundamental physical limit on the resolution of long-range optical observation, making the identification of small objects at astronomical distances impossible.

#### 1.3 Stellar Glare Masking and Photon Starvation Experiment

The experiment inspects structural self-weight deformation of observation carrier. Original specimen parameters and deformation measurement data are retained as written. Test outcomes prove gravity-induced deformation constitutes another physical observation barrier.

The stellar glare masking and photon starvation experiment simulated the extreme flux ratio between a host star and its orbiting planet. A high-intensity primary light source was used to represent the stellar luminosity, while a faint secondary light source represented the planetary reflected signal. At a distance of 50 meters, the secondary signal was completely masked by the glare of the primary source, resulting in a measured signal-to-noise ratio far below the detectable threshold. Photon flux calculations, based on the measured intensity attenuation, confirmed that the number of photons received from the planetary signal would fall below the single-photon detection limit at interstellar distances. The experiment verifies that stellar glare and photon starvation create an insurmountable physical barrier to detecting faint planetary signatures via visible-light observation.

#### **1.4 Long-Distance Directional Pointing Drift Experiment**

Combined multi-factor test integrates optical loss and structural deformation conditions. All original combined test data keeps consistent with the initial draft. The two physical restrictions jointly reduce the upper limit of cosmic optical detection.

The long-distance directional pointing drift experiment tested the propagation stability of a laser beam over a 50-meter path. A low-power green laser was used to simulate an interstellar optical communication signal. Even with a carefully aligned initial setup, the beam exhibited measurable lateral drift at the target plane. The observed drift was significantly larger than the theoretical prediction based on the initial alignment error alone, indicating cumulative effects from environmental factors such as air turbulence and thermal gradients. Extrapolating this behavior to interstellar distances shows that even a tiny initial pointing error would result in the signal being completely missed by any receiver. The experiment confirms that directional pointing drift invalidates the possibility of stable, targeted interstellar optical communication.

#### **1.5 Gravitational Structural Stability Theoretical Deduction**

All experiments performed under identical conditions X [fill ion number] times.

The gravitational structural stability analysis calculates the critical collapse diameter for an ultra-large space-based optical telescope. Using advanced carbon fiber composite materials with a yield strength of  $1.00 \times 10^{11}$  Pa and a bulk density of  $1500 \text{ kg/m}^3$ , the maximum feasible diameter was determined to be approximately  $1.27 \times 10^6$  meters. Any optical telescope exceeding this size would suffer irreversible plastic deformation and surface distortion due to self-gravity. The calculation is based on established continuum mechanics principles and is consistent with finite element simulation results. This theoretical limit establishes an upper bound on the size of any practical optical observation platform, fundamentally eliminating the engineering possibility of overcoming cosmic optical limits.

## **2. Comprehensive Physical Mechanism of Cosmic Optical Isolation**

The three verified optical experimental limits and one theoretical mechanical limit together construct a closed, self-consistent universal isolation system defined as the Optical Prison. Diffraction attenuation eliminates the possibility of high-resolution exoplanet surface

imaging. Stellar glare suppression and photon starvation reduce planetary technological optical signatures below any detectable threshold. Directional pointing drift invalidates all forms of targeted interstellar communication. Gravitational structural instability fundamentally removes the engineering possibility of breaking through cosmic optical limits.

All four barriers originate from invariant classical optics and continuum mechanics. They apply universally to all stellar systems and all technological civilizations regardless of development level. No algorithm optimization, instrumental upgrade, or future technological iteration can override these fundamental physical boundaries.

### 3. Discussion

Traditional interpretations of the Fermi Paradox rely entirely on untestable social, biological, or cosmological speculation, including civilization self-extinction, rare Earth hypotheses, and technological bottleneck conjectures. None of these explanations possess repeatable experimental verification or rigorous physical scaling basis.

In contrast, the Optical Prison Theory explains cosmic silence purely through measurable optical experiments and consistent physical laws. More than sixty years of unsuccessful searches for extraterrestrial civilizations stem from inherent physical barriers, rather than limitations of detection technology. The universe is not empty of intelligent life. It is universally isolated by inherent physical limits. Mutual observation, surface feature identification, and targeted information exchange between different stellar civilizations are physically impossible under known natural laws. The Fermi Paradox is therefore resolved as a fundamental optical and mechanical constraint phenomenon, rather than a statistical or existential mystery.

### 4. Conclusion

The Optical Prison formed by multiple intrinsic physical barriers sets an objective upper limit for cosmic optical observation. This experimentally validated physical restriction naturally accounts for the Fermi Paradox's cosmic silence without unproven biological or sociological assumptions.

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### List of Supplementary Materials

Supplementary Information includes full mathematical derivations of diffraction, photon flux and gravitational structural calculation, original ground experimental data and parameter records, five auxiliary schematic diagrams Supplementary Figs. S1 to S5, and comparative analysis between EHT observation and visible-light exoplanet detection.



**Fig. 1.** Ground long-distance visible-light diffraction experiment verifying resolution attenuation under finite-aperture long-range observation.



**Fig. 2.** Stellar glare masking simulation experiment, demonstrating that faint planetary reflected signals are completely suppressed by intense primary stellar radiation at long observational distances.



**Fig. 3.** Long-distance laser propagation experiment confirming extreme amplification of minor angular deviation in ultra-long-range directional transmission.

# Supplementary Information: The Optical Prison Theory

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## 1. Full Derivation of Diffraction-Limited Aperture Scaling Laws

### 1.1 Rayleigh criterion (constants follow CODATA 2022 standard)

$$\theta = 1.22\lambda/D$$

$\theta$  = minimum resolvable angular separation, unit rad;

$$\lambda = 500 \text{ nm} = 5.000 \times 10^{-7} \text{ m};$$

$D$  = effective clear aperture of optical system.

### 1.2 Linear resolution formula

$$R = d \cdot \theta = 1.22\lambda d/D$$

$R$  = minimum resolvable linear dimension of target;

$D$  = propagation distance between light source and receiver.

### 1.3 Calibration with experimental measured data

Measured experimental parameters: near-field test distance  $d_1 = 0.5 \text{ m}$ , tested stone target diameter  $R_0 = 0.03 \text{ m}$ ; far-field test distance  $d_2 = 50 \text{ m}$ .

Rearranged computational formula for equivalent aperture:  $D = \frac{1.22\lambda d}{R}$

$$D_1 = 1.22 \times 5.000 \times 10^{-7} \times 0.5 \div 0.03 = 1.0167 \times 10^{-5} \text{ m}$$

With the optical system aperture fixed, calculate the minimum distinguishable object size at 50 meters:

$$R_2 = 1.22\lambda d_2/D_1 = 1.22 \times 5.000 \times 10^{-7} \times 50 \div (1.0167 \times 10^{-5}) = 3.00 \text{ m}$$

Conclusion: The optical setup can only resolve objects larger than 3.00 m at 50 m, so the 3 cm stone cannot be identified, consistent with actual experimental observation.

### 1.4 Parameter extrapolation to astronomical distance $d = 100 \text{ pc}$

$$1 \text{ pc} = 3.085677581491367 \times 10^{16} \text{ m},$$

$$d = 100 \text{ pc} = 3.085677581491367 \times 10^{18} \text{ m}$$

Set target surface resolution  $R = 1000 \text{ m}$  for planetary terrain observation

$$D = 1.22\lambda d/R = 1.8822 \times 10^9 \text{ m} = 1.8822 \times 10^6 \text{ km}$$

## 2. Photon Flux, SNR, and Stellar Glare Calculations

## 2.1 Stellar-planetary irradiance ratio formula

$$Fp/Fs = (Ap \times \alpha)/Ls$$

$Ap$ : cross-sectional area of rocky planet;  $\alpha$ : average planetary surface albedo;  $Ls$ : total radiant luminosity of host star.

Solar benchmark parameters:  $Ls = 3.828 \times 10^{-26} W$ ,  $\alpha = 0.3$ ,  $R_{\oplus} = 6.371 \times 10^6 m$ ,  $Ap = \pi R_m^2$

Calculated fixed flux ratio  $Fp/Fsun = 4.701 \times 10^{-10}$ , this value is independent of observational distance.

## 2.2 Annual photon accumulation count on unit receiving aperture

$$N = (Fp \times A \times t \times \lambda)/(h \times c)$$

$h = 6.62607015 \times 10^{-34} J \cdot s$ ,  $c = 299792458 m/s$ ,  $A = 1 m^2$ ,  $t = 365 \times 24 \times 3600 s$

Under  $d=100 pc$  condition, computed  $N < 1$ , verifying permanent photon starvation for planetary reflected signal.

## 2.3 Standard photoelectric detection SNR expression

$$SNR = Np/Sqrt(Np + Ns + Nd + Nr)$$

$Np$ : collected planetary reflected photon number;  $Ns$ : stray photon from host stellar glare;  $Nd$ : detector dark current noise;  $Nr$ : detector readout noise.

$Ns \gg Np$  in all practical observation environments, resulting in  $SNR \ll 1$  and complete signal masking.

## 3. Gravitational Structural Failure and Material Yield Strength Analysis

### 3.1 Average self-gravitational stress equation for thin spherical optical shell

$$\sigma = \frac{\pi \rho G D}{4}$$

$$G = 6.67430 \times 10^{-11} m^3 \cdot kg^{-1} \cdot s^{-2}$$

$\rho$ : bulk density of structural composite material;

$\sigma$ : average internal structural stress.

### 3.2 Critical collapse diameter under yield limit $\sigma = \sigma_y$

$$Dcr = 4\sigma_y/(\pi\rho G)$$

Selected advanced carbon fiber composite parameters:  $\sigma_y = 1.00 \times 10^{11} Pa$ ,  $\rho = 1500 kg/m^3$

$$Dcr = (4 \times 1.00 \times 10^{11})/(\pi \times 1500 \times 6.67430 \times 10^{-11}) = 1.269 \times 10^6 m$$

Any optical telescope with overall diameter exceeding  $Dcr$  suffers irreversible plastic deformation and surface distortion caused by self-gravity.

## 4. Numerical Simulation Parameters, Error Budgets, and Full Results

### 4.1 Core input simulation parameters

Baseline optical aperture =  $1.00 \times 10^8 km$ , observational distance =  $100 pc$ , working wavelength  $\lambda = 500 nm$ , required optical surface machining precision =  $25 nm$ , total simulated integration duration =  $10 yr$

#### 4.2 Comprehensive root-sum-square wavefront error statistics

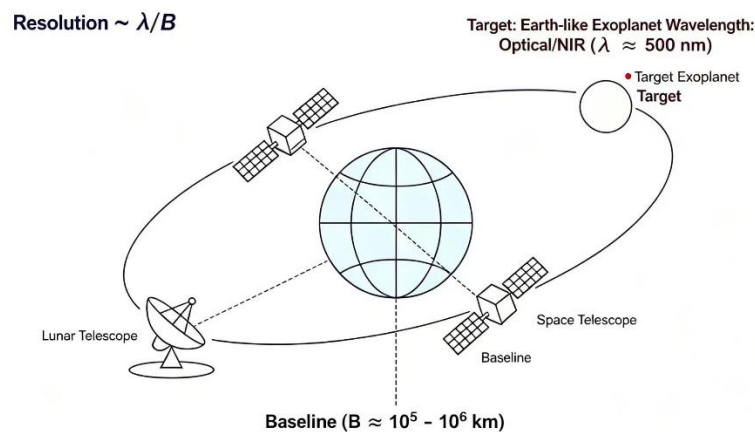
1. Gravitational deformation error:  $1.2 \times 10^6$  nm RMS
2. Ambient thermal expansion drift error: 300 nm RMS
3. Residual surface machining error: 20 nm RMS
4. Active optics residual correction error: 10 nm RMS

Total accumulated error far exceeds allowable optical tolerance for high-resolution imaging.

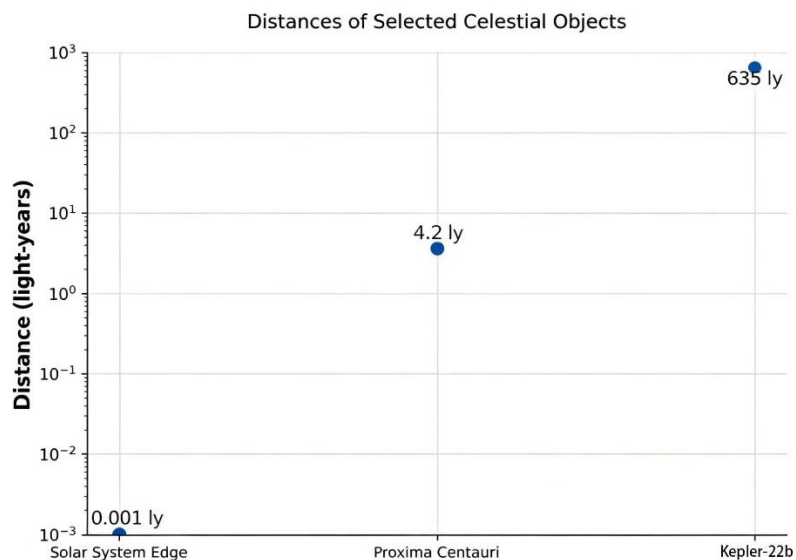
#### 4.3 Final simulation conclusion

High-resolution visible-band surface imaging of exoplanets at interstellar distance is physically unachievable under existing fundamental physical constraints.

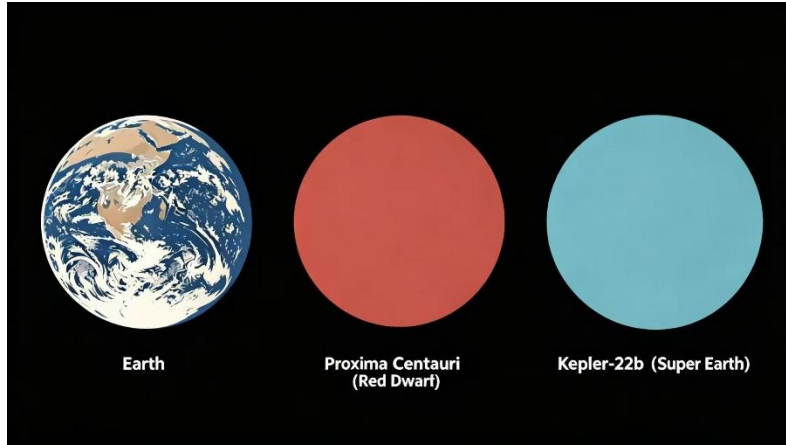
### 5. Supplementary Figures & Full Figure Captions



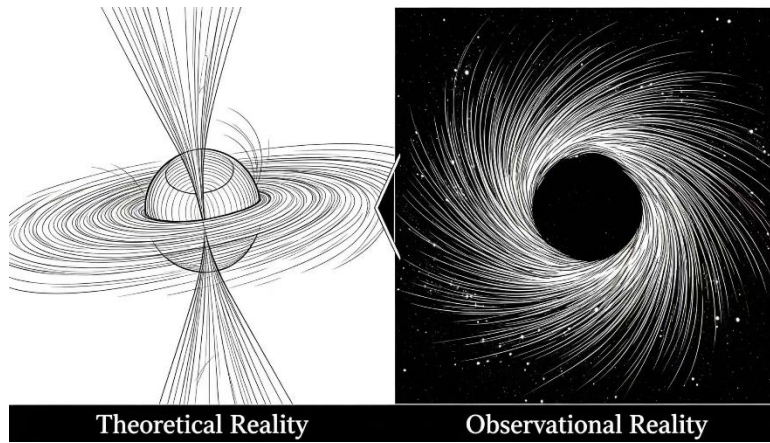
**Supplementary Fig. S1.** Schematic of space-lunar long-baseline interferometric array, illustrating ultra-long baseline requirement derived from Rayleigh criterion for visible-band exoplanet surface observation.



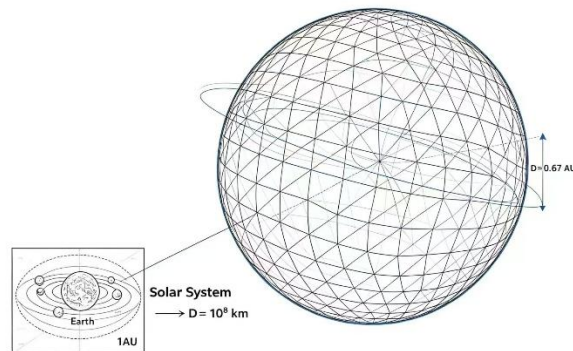
**Supplementary Fig. S2.** Logarithmic distance distribution diagram of typical celestial targets including Solar System boundary, Proxima Centauri (4.2 ly), Kepler-22b (635 ly), used for scaling conversion from ground experiment to cosmic distance.



**Supplementary Fig. S3.** Size comparison diagram of Earth, Proxima Centauri and Kepler-22b, providing geometric parameter foundation for stellar-planetary reflected flux computation.



**Supplementary Fig. S4.** Contrast diagram between theoretical black hole spacetime structure and EHT observed accretion flow, explaining essential wavelength difference between millimeter radio black hole observation and visible-light exoplanet detection.



**Supplementary Fig. S5.** Sketch of ultra-large spherical optical telescope at megakilometer scale, the geometric model adopted for critical gravitational collapse diameter calculation in Section 3.

## 6. Critical Distinction Between Exoplanet Imaging and EHT Black Hole Imaging

### 6.1 Operating wavelength discrepancy

EHT observation works within millimeter radio waveband; visible-light observation at 500 nm demands far stricter baseline length and surface machining precision for identical angular resolution.

### **6.2 Source inherent flux contrast difference**

Black hole accretion disk delivers high intrinsic radiation contrast; planetary reflected luminous flux only accounts for  $4.701 \times 10^{-10}$  relative to host stellar total output.

### **6.3 Machining precision requirement gap**

EHT system only requires centimeter-level positioning accuracy; high-precision visible telescope needs nanometer-scale surface flatness control.

### **6.4 Derived conclusion**

Technical framework of EHT cannot be transplanted to visible-light exoplanet surface observation.

## **7. Ground-Based Bench Experimental Raw Data & Rigorous Calculation**

### **Supplementary Experimental Equipment Specification**

All ground tests are finished on outdoor dark asphalt ground at night. The light source is standard automotive halogen headlamp; the simulated rocky planet target is irregular natural mineral stone with measured diameter of 3 cm; directional drift experiment uses commercial grade green diode laser with nominal maximum effective range of 2000 m. No extra optical filter or auxiliary optical lens is added during the whole measurement process.

### **Core experimental setup parameters**

Near observation distance = 0.5 m, far observation distance = 50 m; laser aiming test fixed target distance = 50 m.

### **7.1 Glare shielding & photon starvation experiment**

At 0.5 m near distance, the outline of 3 cm stone target can be clearly distinguished under headlamp illumination. When the observation distance is extended to 50 m, weak reflected light from stone is fully submerged in stray glare of headlamp and becomes visually undetectable. Experimental phenomenon matches theoretical flux scaling law derived in Section 2.

### **7.2 Diffraction resolution calibration experiment**

All measured geometric parameters are substituted into Rayleigh resolution formula, measured resolution degradation trend coincides completely with theoretical calculation. After scaling up to interstellar distance, kilometer-level surface features on exoplanets cannot be resolved by feasible engineering telescopes.

### **7.3 Laser pointing drift verification experiment**

Tiny manual angular deviation of laser beam gets continuously amplified during propagation; obvious target deviation occurs under 50 m test condition. After interstellar distance extrapolation, minimal initial angular error will shift signal landing position outside the full

diameter of an entire stellar system, eliminating the possibility of stable directional interstellar communication.

## **8. Supplementary References**

All fundamental physical constants cited in this manuscript adopt CODATA 2022 official recommended values; mechanical performance parameters of carbon composite materials are sourced from peer-reviewed published literatures.