1	THE REINTREPRETATION OF THE EINSTEIN DE HAAS
2	EFFECT
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12	ABSTRACT
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14 4 -	This publication contains a mathematical approach for a reinterpretation of the calculation of
15	the magnetic moment for the Einstein de Haas experiment under the assumption of a magne-
16	tic field density from the elaboration "The reinterpretation of the Maxwell equations [1]". The
1/	basis for this is Faraday's unipolar induction, which has proven itself in practice in combinati-
18	on with the calculation rules of vector analysis and differential calculus. The newly calculated
19	"Maxwell equations" offer a generally valid calculation approach for the Einstein de Haas ex-
20	periment and its problem that the difference between measurement and calculation is a factor
21	of 2. This connection is established mathematically in this work.
22	It is shown that the magnetic moment can be derived mathematically by using one of the
23	newly calculated basic equations of electrodynamics from the elaboration "The reinterpretati- $\rightarrow$
24	on of the 'Maxwell equations'[1]". The gradient of the magnetic flux density $\operatorname{grad} B$ and its
25	mathematical consequences regarding the divergence of the magnetic flux density div $\vec{B}$
26	will play an important role here in this essay. By formulating that the trace of the gradient of
27	the magnetic flux density (Sp)grad $\vec{B}$ corresponds to the divergence of the magnetic flux
28	density div $\vec{B}$ a direct connection of the magnetic flux density field itself with the field
29	density of the magnetic flux density is revealed. It also explains and corrects the difference
30	between measurement and calculation in the Einstein de Haas experiment. This is successful
31	because: In this experiment, alternating current and alternating voltage were used to carry out
32	the experiment [2]. Due to this fact, the "Maxwell equations" can be used for calculation and
33	therefore also their new formulation from the article "The reinterpretation of the 'Maxwell
34	equations'[1]".

**1. INTRODUCTION** 36 37 38 The Einstein de Haas experiment was carried out by Albert Einstein (March 14, 1879 - April 39 18, 1955) and Wander Johannes de Haas (March 2, 1878 - April 26, 1960), in 1915. The ex-40 periment showed how a magnetic moment is generated in a body. This effect is now better 41 known as the "Einstein de Haas effect". The interpretation of this effect was that the elementary particles in the body generate a magnetic moment through rotation. The experiment was 42 later repeated several times by different scientists. It turned out that the measurement result of 43 the experiment is generally a factor of 2 larger than the corresponding calculation. 44 45 A solution to this problem is offered in the paper "The reinterpretation of the 'Maxwell equations'[1]". Therefore, the elaboration "The reinterpretation of the Maxwell equation'[1]" 46 47 serves as the basis for this work. In particular, the newly formulated approach to induction and the associated magnetic field density are the core of the following chapters. Only the 48 49 solution to the problem of factor 2, between measurement and calculation for the Einstein de 50 Haas experiment, is focused on. 51 52 2. IDEAS AND METHODS 53 54 2.1 IDEA FOR REINTERPRETING THE "EINSTEIN DE HAAS EFFECT" 55 56 First of all, it must be clarified that "The reinterpretation of the Einstein de Haas effect" is not 57 58 a reinterpretation but rather a reformulation of the calculation on the topic, since the effect itself does not need to be reinterpreted. The basic idea for the development: "The reinterpreta-59 60 tion of the Einstein de Haas effect" is based on carrying out of the following experiments: 61 62 1. Albert Einstein und Wander Johannes de Haas, 1915, Verhandlungen der Deutschen Physi-63 kalischen Gesellschaft, Bad Honnef, Experimenteller Nachweis der Ampèreschen Molekular-64 ströme<sup>[2]</sup>. 65 66 2. Polykarp Kusch und Henry M. Foley, 1955, Physical Review, USA, The Magnetic Moment of the Electron 67 68

- 69 3. Samuel Goudsmit und Georg Uhlenbeck, 1925, Zeitschrift für Physik, Deutschland, Erset-
- 70 zung der Hypothese vom unmechanischen Zwang durch eine Forderung bezüglich des inne-
- 71 ren Verhaltens jedes einzelnen Elektrons
- 73 Based on the elaboration of "The reinterpretation of the 'Maxwell equations'[1]" and the asso-
- 74 ciated mathematical requirement of a magnetic field density, the magnetic moment can now
- 75 be reformulated.
- 76 All physical and mathematical descriptions used in this work are listed below.
- $\vec{E}$  = electric field strength
- $\vec{v}$  = velocity
- $\vec{B}$  = magnetic flux density
- $\times$  = cross product
- $\vec{s} = \text{distance}$
- t = time
- $\delta = delta$
- 85 rot = rotation
- div = divergence
- grad = gradient
- $\vec{m}$  = magnetic moment
- $\vec{m}_{(t)}$  = time-dependent magnetic moment
- I = electrical current strength
- $i_{(t)}$  = electrical current strength (alternating current)
- U = electrical voltage
- $u_{(t)}$  = electric voltage (alternating voltage)
- R = electrical resistance
- $\vec{A}$  = area
- Sp = trace/track
- 98 Unipolar induction according to Farady:
- $99 \quad \vec{E} = \vec{v} \times \vec{B} \tag{2.1.1}$
- 101 Magnetic moment:

$$102 \quad \vec{m} = I \cdot \vec{A} \tag{2.1.2}$$

104	
105	2.2 BASICS OF VECTOR CALCULATION
106	
107	In order to be able to derive the equation for the induction from the newly formulated equati-
108	on for the reformulation of the Einstein de Haas experiment, the basics of vector calculation
109	used for this are described in this chapter.
110	First of all, three meta-vectors $\vec{a}$ , $\vec{b}$ and $\vec{c}$ are introduced at this point. The three
111	meta-vectors will be used in the following basic mathematical description. In Equation 2.2.1,
112	these three meta-vectors are used to represent the cross product.
113	
114	$\vec{c} = \vec{a} \times \vec{b} \tag{2.2.1}$
115	
116	In equation 2.2.1, the rotation operator ( rot ) is now applied to both sides of the equation.
117	This creates equation 2.2.2.
118	
119	$\operatorname{rot} \ \vec{c} = \operatorname{rot} \ (\vec{a} \times \vec{b}) \tag{2.2.2}$
120	
121	Now the right-hand side of equation 2.2.2 is rewritten according to the calculation rules of
122	vector calculation. This results in equation 2.2.3.
123	
124	$\operatorname{rot} \vec{c} = \operatorname{rot}(\vec{a} \times \vec{b}) = (\operatorname{grad} \vec{a}) \vec{b} - (\operatorname{grad} \vec{b}) \vec{a} + \vec{a} \operatorname{div} \vec{b} - \vec{b} \operatorname{div} \vec{a} $ (2.2.3)
125	
126	On the right side of equation 2.2.3 two vector gradients arise, to be exact $(\operatorname{grad} \vec{a})$ and
127	$(\operatorname{grad} \vec{b})$ . In addition, two vector divergences arise, to be exact $(\operatorname{div} \vec{a})$ and $(\operatorname{div} \vec{b})$ .
128	From equation 2.2.3, for equation 2.1.1 follows, by applying the rotation operator ( rot ),
129	the equation 2.2.4.
130	
131	$\vec{E} = \vec{v} \times \vec{B} \tag{2.1.1}$
132	
133	$\operatorname{rot} \vec{E} = (\operatorname{grad} \vec{v}) \ \vec{B} - (\operatorname{grad} \vec{B})\vec{v} + \vec{v} \ \operatorname{div} \vec{B} - \vec{B} \ \operatorname{div} \vec{v} $ (2.2.4)
134	
135	The relationship between the expressions $(\operatorname{grad} \vec{a})$ and $\operatorname{div} \vec{a}$ is described by equation
136	2.2.5.
137	
138	$(Sp)(\operatorname{grad} \vec{a}) = \operatorname{div} \vec{a}$ (2.2.5)

140 The connection of equation 2.2.5 also applies to the connections of equations 2.2.6, 2.2.7 and 2.2.8. Equations 2.2.7 and 2.2.8 refer to equation 2.2.4. 141 142  $(Sp)(\operatorname{grad} \vec{b}) = \operatorname{div} \vec{b}$ 143 (2.2.6)144  $(Sp)(\operatorname{grad} \vec{B}) = \operatorname{div} \vec{B}$ 145 (2.2.7)146  $(Sp)(\operatorname{grad} \vec{v}) = \operatorname{div} \vec{v}$ 147 (2.2.8)148 Equation 2.2.7 will still play an important role in the reformulation of the magnetic pole mo-149 ment  $\vec{m}$ . First, however, the magnetic pole moment  $\vec{m}$  is explained in Chapter 2.3. 150 151 **2.3 THE MAGNETIC POLE MOMENT** 152 153 154 Since there are a number of formal descriptions of the magnetic pole moment  $\vec{m}$ , of which only the one used by Einstein and de Haas is needed to meet the goal of this work, only this 155 156 will be discussed [2]. Equation 2.1.2 describes this magnetic pole moment  $\vec{m}$ . In equation 2.1.2, I stands for the electric current and  $\vec{A}$  stands for the area that is penetratesd by 157 the magnetic field in the direction of the magnetic pole moment  $\vec{m}$ . 158 159  $\vec{m} = I \cdot \vec{A}$ 160 (2.1.2)161 The formulation described in Equation 2.1.2 states that the magnetic pole moment  $\vec{m}$ 162 is calculated by multiplying the area  $\vec{A}$  that is penetrated by the magnetic field with the elec-163 164 tric current I that encloses this area. However, in the Einstein de Haas experiment an alternating current  $i_{(t)}$  was used, which 165 means that equation 2.1.2 must be reformulated into equation 2.3.1. 166 167  $\vec{\mathbf{m}}_{(t)} = \mathbf{i}_{(t)} \cdot \vec{A}$ (2.3.1)168 169 170 Starting from equation 2.3.1, it will now be shown why only half of the measured value for the magnetic pole moment  $\vec{m}$  can be calculated by using the "Maxwell equations". For 171

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this purpose, the newly formulated "Maxwell equations" from the elaboration "The reinterpre-

tation of the 'Maxwell equations'[1]" will be used, which results in a calculated value for the 173 time-dependent magnetic pole moment  $\vec{m}_{(t)}$ , that also corresponds to the actual measured 174 value for the time-dependent magnetic pole moment  $\vec{\mathbf{m}}_{(t)}$ . 175

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## 2.4 DERIVATION OF THE FORMULA FOR THE MAGNETIC MOMENT

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In the following chapters, the time-dependent magnetic moment  $\vec{\mathbf{m}}_{(t)}$  is connected to Hea-179 viside's "Maxwell equations", specifically to the law of induction. This is done in order to cre-180 ate the conditions for subsequently connecting the time-dependent magnetic moment  $\vec{\mathbf{m}}_{(t)}$ 181 with the newly formulated "Maxwell equations" from the elaboration: "The reinterpretation of 182 the 'Maxwell equations'[1]". These new "Maxwell equations" can be used to explain why the 183 184 measurement result from the experiments on the time-dependent magnetic moment  $\vec{\mathbf{m}}_{(t)}$ 

assumes twice the value from the associated calculation. 185

The derivation adequately explains this discrepancy by introducing a magnetic field density 186  $(\operatorname{div} \vec{B})$ . 187

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- 189

# 2.4.1 THE MAGNETIC MOMENT AND "THE MAXWELL EQUATIONS"

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In order to explain the time-dependent magnetic moment  $\vec{\mathbf{m}}_{(t)}$ , a simple technical setup is 191 first used here theoretically, in which the electric current and the area play a role. Considering 192 a simple loop of wire through which an electric current flows, this current creates a magnetic 193 field, twisted at a 90° angle, around and through the loop of the wire. The strength of this ma-194 195 gnetic field depends on the strength of the electric current and the size of the area of the wire loop. The area enclosed by the wire loop therefore contains a part of the magnetic field gene-196 rated by the electric current, to be exact the part that is relevant for calculating the magnetic 197 moment. The magnetic moment is now a vector that is perpendicular, at a 90° angle, to the 198 surface enclosed by the conductor loop. If the conductor loop is now subjected to an alterna-199 ting current, both the magnetic field and the magnetic moment change direction depending on 200 time, with the frequency of the alternating current by 180°. In order to derive the time-depen-201 dent magnetic moment  $\vec{\mathbf{m}}_{(t)}$ , a comparison is made at this point. The starting point for the 202 derivation of the magnetic moment will be equation 2.3.1 in combination with the "Maxwell 203 equations", first according to the well-known simplified formulation by Oliver Heaviside and 204 then according to the formulation from the elaboration "The reinterpretation of the 'Maxwell 205 equations'[1]". The differences between the two formulations are highlighted. In a first step, 206

however, a formulation must be found that connects the "Maxwell equations" with the timedependent magnetic moment  $\vec{\mathbf{m}}_{(t)}$ . To do this, the basic formula for the magnetic moment from equation 2.3.1 is used as an introduction.

211 
$$\vec{\mathbf{m}}_{(t)} = \dot{\mathbf{i}}_{(t)} \cdot \vec{A}$$
 (2.3.1)

212

213 If Ohm's law applied to the time-dependent electric current  $i_{(t)}$ , the expression from equa-214 tion 2.4.1 is created.

215

216 
$$i_{(t)} = \frac{u_{(t)}}{R}$$
 (2.4.1)

217

The time-dependent electrical voltage  $u_{(t)}$  can now be reformulated as  $-\frac{\delta \vec{B}}{\delta t} \cdot \vec{A}$ . It is assumed here that the area  $\vec{A}$  enclosed by the conductor is constant and points vectorially in the same direction as the resulting time-dependent magnetic flux density  $\frac{\delta \vec{B}}{\delta t}$ . If this expression for the time-dependent voltage  $U_{(t)}$  is inserted into equation 2.4.1, equation 2.4.2 results.

223

224 
$$\mathbf{i}_{(t)} = \frac{\left(-\frac{\delta \vec{B}}{\delta t} \cdot \vec{A}\right)}{R}$$
(2.4.2)

225

Now the formulation for the time-dependent electric current  $\mathbf{i}_{(t)}$  from equation 2.4.2 can be inserted back into equation 2.3.1 for the time-dependent magnetic moment  $\vec{\mathbf{m}}_{(t)}$ , resulting in equation 2.4.3.

230 
$$\vec{\mathbf{m}}_{(t)} = \left(\frac{-\delta \vec{B} \cdot \vec{A}}{R}\right) \cdot \vec{A}$$
 (2.4.3)  
231

233 to the "Maxwell equations". Here this happens specifically using the expression  $-\frac{\delta \vec{B}}{\delta t}$ . 234 This expression represents part of the law of induction.

At this point the time-dependent magnetic moment  $\mathbf{m}_{(t)}$  would be sufficiently described, taking into account the "Maxwell equations" according to Heaviside. In the next chapter, equation 2.4.3 is used and the calculation for the time-dependent magnetic moment  $\vec{\mathbf{m}}_{(t)}$  is carried out, taking into account the newly formulated "Maxwell equations" from the elaboration "The reinterpretation of the 'Maxwell equations'[1]" improved.

2.4.2 THE MAGNETIC MOMENT AND "THE REINTERPRETATION OF THE

'MAXWELL-EQUATIONS'''

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#### 241 242

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In the last chapter (Chapter 2.4.1) the magnetic moment was connected to the "Maxwell equations" according to Oliver Heaviside. Equation 2.4.3 shows this fact. In connection with the "Maxwell equations" according to Heaviside, the time-dependent magnetic moment  $\vec{m}_{(t)}$  is adequately described by equation 2.4.3, but not according to the newly formulated "Maxwell equations" from the elaboration "The reinterpretation of the 'Maxwell -Equations'[1]". Equation 2.4.3 therefore serves as the basis for this chapter. The term

250 
$$-\frac{\delta B}{\delta t}$$
 in particular will undergo a mathematical and physical reformulation.

251

252 
$$\mathbf{m}_{(t)} = \left(\frac{\left(-\frac{\delta B}{\delta t} \cdot \vec{A}\right)}{R}\right) \cdot \vec{A}$$
(2.4.3)

253

First, the term  $-\frac{\delta \vec{B}}{\delta t}$  is isolated from equation 2.4.3 and Heaviside's induction law is derived from it. This is shown by equation 2.4.4.

256

257 
$$\operatorname{rot} \vec{E} = -\frac{\delta \vec{B}}{\delta t}$$
 (2.4.4)

258

259 Since  $-\frac{\delta \vec{B}}{\delta t}$  represents a vector in equation 2.4.4, it can also be represented in its compo-260 nent notation. This is represented by the formulation from Equation 2.4.5.

262 rot 
$$\vec{E} = -\left(\frac{\frac{\delta B_x}{\delta t}}{\frac{\delta B_y}{\delta t}}\right)$$
 (2.4.5)

264 In the next step, the individual components  $\frac{\delta B_x}{\delta t}$ ,  $\frac{\delta B_y}{\delta t}$  and  $\frac{\delta B_z}{\delta t}$  from equation 265 2.4.5 are each added twice to the value 0. This is shown by equation 2.4.6.

267 
$$\operatorname{rot} \vec{E} = - \begin{pmatrix} \frac{\delta B_x}{\delta t} + 0 + 0\\ 0 + \frac{\delta B_y}{\delta t} + 0\\ 0 + 0 + \frac{\delta B_z}{\delta t} \end{pmatrix}$$
(2.4.6)

269 If the individual terms from equation 2.4.6 are now multiplied by the value 1, equation 2.4.7

270 results. The value 1 is equated here with the expressions  $\frac{\delta x}{\delta x}$ ,  $\frac{\delta y}{\delta y}$  and  $\frac{\delta z}{\delta z}$ .

272 
$$\operatorname{rot} \vec{E} = - \begin{pmatrix} \frac{\delta B_x}{\delta t} \cdot \frac{\delta x}{\delta x} + 0 \cdot \frac{\delta y}{\delta y} + 0 \cdot \frac{\delta z}{\delta z} \\ 0 \cdot \frac{\delta x}{\delta x} \cdot + \frac{\delta B_y}{\delta t} \cdot \frac{\delta y}{\delta y} + 0 \cdot \frac{\delta z}{\delta z} \\ 0 \cdot \frac{\delta x}{\delta x} + 0 \cdot \frac{\delta y}{\delta y} + \frac{\delta B_z}{\delta t} \cdot \frac{\delta z}{\delta z} \end{pmatrix}$$

$$(2.4.7)$$

274 If the expression from equation 2.4.8 is now applied to equation 2.4.7, equation 2.4.9 is crea-275 ted.

277 
$$0 = \frac{\delta B_x}{\delta t} = \frac{\delta B_y}{\delta t} = \frac{\delta B_z}{\delta t}$$
(2.4.8)

279 
$$\operatorname{rot} \vec{E} = - \begin{pmatrix} \frac{\delta B_x}{\delta t} \cdot \frac{\delta x}{\delta x} + \frac{\delta B_x}{\delta t} \cdot \frac{\delta y}{\delta y} + \frac{\delta B_x}{\delta t} \cdot \frac{\delta z}{\delta z} \\ \frac{\delta B_y}{\delta t} \cdot \frac{\delta x}{\delta x} + \frac{\delta B_y}{\delta t} \cdot \frac{\delta y}{\delta y} + \frac{\delta B_y}{\delta t} \cdot \frac{\delta z}{\delta z} \\ \frac{\delta B_z}{\delta t} \cdot \frac{\delta x}{\delta x} + \frac{\delta B_z}{\delta t} \cdot \frac{\delta y}{\delta y} + \frac{\delta B_z}{\delta t} \cdot \frac{\delta z}{\delta z} \end{pmatrix}$$
(2.4.9)

281 In the next step, the velocity  $\vec{v}$  is solved from equation 2.4.9 and equation 2.4.10 is crea-

282 ted. The velocity vector 
$$\vec{v}$$
 can also be expressed as  $\frac{\delta \vec{s}}{\delta t}$  and therefore also as  $\begin{pmatrix} \frac{\delta x}{\delta t} \\ \frac{\delta y}{\delta t} \\ \frac{\delta z}{\delta t} \end{pmatrix}$ 

.

283

$$284 \quad \operatorname{rot} \vec{E} = - \begin{pmatrix} \frac{\delta B_x}{\delta x} \cdot \frac{\delta x}{\delta t} + \frac{\delta B_x}{\delta y} \cdot \frac{\delta y}{\delta t} + \frac{\delta B_x}{\delta z} \cdot \frac{\delta z}{\delta t} \\ \frac{\delta B_y}{\delta x} \cdot \frac{\delta x}{\delta t} + \frac{\delta B_y}{\delta y} \cdot \frac{\delta y}{\delta t} + \frac{\delta B_y}{\delta z} \cdot \frac{\delta z}{\delta t} \\ \frac{\delta B_z}{\delta x} \cdot \frac{\delta x}{\delta t} + \frac{\delta B_z}{\delta y} \cdot \frac{\delta y}{\delta t} + \frac{\delta B_z}{\delta z} \cdot \frac{\delta z}{\delta t} \end{pmatrix}$$
(2.4.10)

285

In a final step, the velocity vector  $\vec{v}$  in equation 2.4.10 is decoupled from the overall vector. This is shown in equation 2.4.11.

288

289 rot 
$$\vec{E} = - \begin{pmatrix} \frac{\delta B_x}{\delta x} & \frac{\delta B_x}{\delta y} & \frac{\delta B_x}{\delta z} \\ \frac{\delta B_y}{\delta x} & \frac{\delta B_y}{\delta y} & \frac{\delta B_y}{\delta z} \\ \frac{\delta B_z}{\delta x} & \frac{\delta B_z}{\delta y} & \frac{\delta B_z}{\delta z} \end{pmatrix} \begin{pmatrix} \frac{\delta x}{\delta t} \\ \frac{\delta y}{\delta t} \\ \frac{\delta z}{\delta t} \end{pmatrix}$$
(2.4.11)

290

291 The velocity vector  $\vec{v}$  and the gradient of the magnetic flux density (grad  $\vec{B}$ ) are crea-292 ted in equation 2.4.11. The simplified notation is shown in equation 2.4.12.

294 rot 
$$\vec{E} = -(\operatorname{grad} \vec{B})\vec{v}$$
 (2.4.12)

Equation 2.4.12 describes the unsimplified form of Heaviside's induction law. If this formulation is now compared with equation 2.2.4, it is noticeable that equation 2.4.12 is mathematically incomplete.

299

300 rot 
$$\vec{E} = -(\operatorname{grad} \vec{B})\vec{v}$$
 (2.4.12)

301

302 rot 
$$\vec{E} = (\operatorname{grad} \vec{v}) \vec{B} - (\operatorname{grad} \vec{B})\vec{v} + \vec{v} \operatorname{div} \vec{B} - \vec{B} \operatorname{div} \vec{v}$$
 (2.2.4)  
303

Apparently, three of the five terms in equation 2.2.4 must be interpreted with the value 0 in order to fulfill the requirements from equation 2.4.12, Heaviside's induction law. Due to the mathematical formulation from equations 2.2.7 and 2.2.8, it must be stated at this point that it is not mathematically possible to interpret these three terms with the value 0. At least three terms from equation 2.2.4 must therefore have a value that is not equal to 0 if rot  $\vec{E}$  is to deliver a value that is not equal to 0.

310

311 
$$(Sp)(\operatorname{grad} \vec{B}) = \operatorname{div} \vec{B}$$
 (2.2.7)

312

313 
$$(Sp)(\operatorname{grad} \vec{v}) = \operatorname{div} \vec{v}$$
 (2.2.8)

314

If equations 2.2.7 and 2.2.8 are considered, it must be noted that two terms in equation 2.2.4 are connected to each other. On the one hand the term  $(\mathbf{grad} \vec{B})\vec{v}$  with the term  $\vec{v} \ \mathbf{div} \vec{B}$  and on the other hand the term  $(\mathbf{grad} \vec{v})\vec{B}$  with the term  $\vec{B} \ \mathbf{div} \vec{v}$ . The second pair of terms around the velocity gradient  $(\mathbf{grad} \vec{v})$  describes a formulation for the change in spatial content, for example material deformation. The first pair of terms around the gradient of the magnetic flux density  $(\mathbf{grad} \vec{B})$ , on the other hand, describes, for example, a distortion or density states in the magnetic flux density  $\vec{B}$ .

322 If the volume is not subject to such influences, for example there is no material deformation 323 in possible tests, the influence of the velocity gradient (grad  $\vec{v}$ ) and the velocity diver-324 gence div  $\vec{v}$  can be assumed to be 0. This results in equation 2.4.13. However, it must be 325 expressly pointed out at this point that these two terms must not generally be assumed to have 326 the value 0.

328 rot 
$$\vec{E} = 0 - (\operatorname{grad} \vec{B})\vec{v} + \vec{v} \operatorname{div} \vec{B} - 0$$
 (2.4.13)

330 
$$(Sp)(\operatorname{grad} \vec{B}) = \operatorname{div} \vec{B}$$
 (2.2.7)

331

The two remaining terms, i.e.  $(\mathbf{grad}\,\vec{B})\vec{v}$  and  $\vec{v}\,\mathbf{div}\,\vec{B}$ , are directly connected to each other by the mathematical requirement from equation 2.2.7. This was sufficiently explained in the paper "The reinterpretation of the 'Maxwell equations'[1]". The elements of the trace (Sp) of the gradient of the magnetic flux density  $(\mathbf{grad}\,\vec{B})$  are the elements that form

the basis for the expression  $-\frac{\delta \vec{B}}{\delta t}$  and, according to equation 2.2.7, also describe the divergence of the magnetic flux density  $\mathbf{div} \vec{B}$ . To illustrate this, the term  $(\mathbf{grad} \vec{B})\vec{v}$ from equation 2.4.13 is presented in column notation. This is shown in equation 2.4.14.

340 rot 
$$\vec{E} = 0 - \begin{pmatrix} \frac{\delta B_x}{\delta x} & \frac{\delta B_x}{\delta y} & \frac{\delta B_x}{\delta z} \\ \frac{\delta B_y}{\delta x} & \frac{\delta B_y}{\delta y} & \frac{\delta B_y}{\delta z} \\ \frac{\delta B_z}{\delta x} & \frac{\delta B_z}{\delta y} & \frac{\delta B_z}{\delta z} \end{pmatrix} \begin{vmatrix} \frac{\delta x}{\delta t} \\ \frac{\delta y}{\delta t} \\ \frac{\delta z}{\delta t} \end{vmatrix} + \vec{v} \operatorname{div} \vec{B} - 0$$
 (2.4.14)

341

The components marked in Equation 2.4.14, i.e.  $\frac{\delta B_x}{\delta x}$ ,  $\frac{\delta B_y}{\delta y}$  and  $\frac{\delta B_z}{\delta z}$ , when added together, form the trace (Sp) of the gradient of the magnetic flux density  $(\text{grad } \vec{B})$  and thus also its field density  $\mathbf{div} \vec{B}$ . Looking back at Equation 2.4.11, these are also the components that in Heaviside's induction law, define the value  $-\frac{\delta \vec{B}}{\delta t}$ . This specifically means that if the trace of the gradient of the magnetic flux density  $(Sp)(\text{grad } \vec{B})$  has a value that is not equal to 0, then mathematically the divergence of the magnetic flux density  $\mathbf{div} \vec{B}$ must also have a value that is not equal to 0.

350 
$$\operatorname{rot} \vec{E} = - \begin{pmatrix} \frac{\delta B_x}{\delta x} & \frac{\delta B_x}{\delta y} & \frac{\delta B_x}{\delta z} \\ \frac{\delta B_y}{\delta x} & \frac{\delta B_y}{\delta y} & \frac{\delta B_y}{\delta z} \\ \frac{\delta B_z}{\delta x} & \frac{\delta B_z}{\delta y} & \frac{\delta B_z}{\delta z} \end{pmatrix} \begin{pmatrix} \frac{\delta x}{\delta t} \\ \frac{\delta y}{\delta t} \\ \frac{\delta z}{\delta t} \end{pmatrix}$$

$$(2.4.11)$$

352 If the term  $\vec{v} \, \text{div} \, \vec{B}$  is now represented in equation 2.4.14 in its column notation or com-353 ponent notation, this results in equation 2.4.15.

354

$$355 \quad \operatorname{rot} \vec{E} = 0 - \begin{pmatrix} \frac{\delta B_x}{\delta x} & \frac{\delta B_x}{\delta y} & \frac{\delta B_x}{\delta z} \\ \frac{\delta B_y}{\delta x} & \frac{\delta B_y}{\delta y} & \frac{\delta B_y}{\delta z} \\ \frac{\delta B_z}{\delta x} & \frac{\delta B_z}{\delta y} & \frac{\delta B_z}{\delta z} \end{pmatrix} \begin{vmatrix} \frac{\delta x}{\delta t} \\ \frac{\delta y}{\delta t} \\ \frac{\delta z}{\delta t} \end{vmatrix} + \begin{pmatrix} \frac{\delta x}{\delta t} \\ \frac{\delta y}{\delta t} \\ \frac{\delta z}{\delta t} \end{vmatrix} + \begin{pmatrix} \frac{\delta B_x}{\delta t} \\ \frac{\delta y}{\delta t} \\ \frac{\delta z}{\delta t} \end{vmatrix} (\frac{\delta B_x}{\delta x} + \frac{\delta B_y}{\delta y} + \frac{\delta B_z}{\delta z}) - 0 \quad (2.4.15)$$

356

357 Since the divergence of the magnetic flux density div  $\vec{B}$  is a single numerical value consis-358 ting of an addition of the components  $\frac{\delta B_x}{\delta x}$ ,  $\frac{\delta B_y}{\delta y}$  and  $\frac{\delta B_z}{\delta z}$ , it must be multiplied 359 by each element of the velocity vector  $\vec{v}$ . This circumstance is shown in equation 2.4.16. 360

$$361 \quad \operatorname{rot} \vec{E} = 0 - \left| \frac{\delta B_x}{\delta x} \frac{\delta B_x}{\delta y} \frac{\delta B_x}{\delta z}}{\delta y} \frac{\delta B_y}{\delta z}}{\delta y} \frac{\delta B_z}{\delta z}} \right| \frac{\delta x}{\delta t}}{\delta t} + \left| \frac{(\delta x)(\delta B_x}{\delta x} + \frac{\delta B_y}{\delta y} + \frac{\delta B_z}{\delta z})}{(\delta y)(\delta x)} - 0 \quad (2.4.16)$$

362

363 If equation 2.4.16 is now considered under the assumption that the magnetic flux density 364  $\vec{B}$  is not subject to deformation, distortion or torsion, equation 2.4.16 can be simplified to 365 equation 2.4.17. It must also be made clear at this point that this assumption cannot be made 366 in principle, since there are definitely circumstances under which a deformation, distortion or 367 torsion can arise in the magnetic flux density  $\vec{B}$ .

$$369 \quad \operatorname{rot} \vec{E} = 0 - \left| \begin{pmatrix} \frac{\delta B_x}{\delta x} & 0 & 0 \\ 0 & \frac{\delta B_y}{\delta y} & 0 \\ 0 & 0 & \frac{\delta B_z}{\delta z} \end{pmatrix} \left| \begin{pmatrix} \frac{\delta x}{\delta t} \\ \frac{\delta y}{\delta t} \\ \frac{\delta z}{\delta t} \end{pmatrix} + \left| \begin{pmatrix} (\frac{\delta x}{\delta t}) (\frac{\delta B_x}{\delta x} + \frac{\delta B_y}{\delta y} + \frac{\delta B_z}{\delta z}) \\ (\frac{\delta y}{\delta t}) (\frac{\delta B_x}{\delta x} + \frac{\delta B_y}{\delta y} + \frac{\delta B_z}{\delta z}) \\ (\frac{\delta z}{\delta t}) (\frac{\delta z}{\delta x} + \frac{\delta B_y}{\delta y} + \frac{\delta B_z}{\delta z}) \right| = 0 \quad (2.4.17)$$

If equation 2.4.17 now calculates the elements of the velocity vectors, i.e.  $\frac{\delta x}{\delta t}$ ,  $\frac{\delta y}{\delta t}$  and 

 $\frac{\delta z}{\delta t}$ , with the elements of the magnetic flux density, i.e.  $\frac{\delta B_x}{\delta x}$ ,  $\frac{\delta B_y}{\delta y}$  and  $\frac{\delta B_z}{\delta z}$ , 

mathematically correctly, equation 2.4.18 is created.

$$375 \quad \operatorname{rot} \vec{E} = 0 - \left| \begin{array}{c} \frac{\delta B_x}{\delta x} \frac{\delta x}{\delta t} + 0 \frac{\delta y}{\delta t} + 0 \frac{\delta z}{\delta t} \\ 0 \frac{\delta x}{\delta t} + \frac{\delta B_y}{\delta y} \frac{\delta y}{\delta t} + 0 \frac{\delta z}{\delta t} \\ 0 \frac{\delta x}{\delta t} + 0 \frac{\delta y}{\delta t} + \frac{\delta B_z}{\delta z} \frac{\delta z}{\delta t} \end{array} \right| + \left| \begin{array}{c} \frac{\delta B_x}{\delta x} \frac{\delta x}{\delta t} + \frac{\delta B_y}{\delta y} \frac{\delta x}{\delta t} + \frac{\delta B_z}{\delta z} \frac{\delta x}{\delta t} \\ \frac{\delta B_x}{\delta x} \frac{\delta y}{\delta t} + \frac{\delta B_y}{\delta y} \frac{\delta y}{\delta t} + \frac{\delta B_z}{\delta z} \frac{\delta y}{\delta t} \\ \frac{\delta B_x}{\delta x} \frac{\delta y}{\delta t} + \frac{\delta B_y}{\delta y} \frac{\delta y}{\delta t} + \frac{\delta B_z}{\delta z} \frac{\delta y}{\delta t} \\ \frac{\delta B_x}{\delta x} \frac{\delta z}{\delta t} + \frac{\delta B_y}{\delta y} \frac{\delta z}{\delta t} + \frac{\delta B_z}{\delta z} \frac{\delta y}{\delta t} \\ - 0 \quad (2.4.18)$$

If equation 2.4.18 now assumes that there are no spatial distortions, deformations or torsions, only the expressions that contain  $\frac{\delta x}{\delta x}$ ,  $\frac{\delta y}{\delta y}$  and  $\frac{\delta z}{\delta z}$  remain. This circumstance is shown in equation 2.4.19. Here, too, it must be made clear that this assumption cannot be made in principle, as there are circumstances under which spatial deformation, distortion or torsion can be assumed.

$$383 \quad \operatorname{rot} \vec{E} = 0 - \left| \begin{pmatrix} \frac{\delta B_x}{\delta x} \frac{\delta x}{\delta t} + 0 + 0 \\ 0 + \frac{\delta B_y}{\delta y} \frac{\delta y}{\delta t} + 0 \\ 0 + \frac{\delta B_z}{\delta z} \frac{\delta z}{\delta t} \end{pmatrix} + \left| \begin{pmatrix} \frac{\delta B_x}{\delta x} \frac{\delta x}{\delta t} + 0 + 0 \\ 0 + \frac{\delta B_y}{\delta y} \frac{\delta y}{\delta t} + 0 \\ 0 + \frac{\delta B_z}{\delta z} \frac{\delta z}{\delta t} \\ 0 + 0 + \frac{\delta B_z}{\delta z} \frac{\delta z}{\delta t} \\ \end{pmatrix} - 0 \quad (2.4.19)$$

If equation 2.4.19 is further simplified, equation 2.4.20 is created. 

$$387 \quad \operatorname{rot} \vec{E} = 0 - \left| \frac{\frac{\delta B_x}{\delta x} \frac{\delta x}{\delta t}}{\frac{\delta B_y}{\delta y} \frac{\delta y}{\delta t}}{\frac{\delta B_z}{\delta z} \frac{\delta z}{\delta t}} \right| + \left| \frac{\frac{\delta B_x}{\delta x} \frac{\delta x}{\delta t}}{\frac{\delta B_y}{\delta y} \frac{\delta y}{\delta t}} \right| - 0 \quad (2.4.20)$$

390 If the elements  $\frac{\delta x}{\delta x}$ ,  $\frac{\delta y}{\delta y}$  and  $\frac{\delta z}{\delta z}$  are shortened in equation 2.4.20, this results in

**391** equation 2.4.21.

392

393 rot 
$$\vec{E} = 0 - \left(\frac{\delta B_x}{\delta t}\\ \frac{\delta B_y}{\delta t}\\ \frac{\delta B_z}{\delta t}\right) + \left(\frac{\delta B_x}{\delta t}\\ \frac{\delta B_z}{\delta t}\\ \frac{\delta B_z}{\delta t}\right) - 0$$
 (2.4.21)

394

**395** Further simplifying equation 2.4.21 results in equation 2.4.22.

396

397 rot 
$$\vec{E} = -2 \cdot \begin{pmatrix} \frac{\delta B_x}{\delta t} \\ \frac{\delta B_y}{\delta t} \\ \frac{\delta B_z}{\delta t} \end{pmatrix}$$
 (2.4.22)

398

In the last step, the column notation of the vector is transferred to the arrow notation. This re-sults in equation 2.4.23.

401

402 rot 
$$\vec{E} = -2 \cdot \frac{\delta \vec{B}}{\delta t}$$
 (2.4.23)

403

404 rot 
$$\vec{E} = -\frac{\delta \vec{B}}{\delta t}$$
 (2.4.4)

405

406 A comparison of the result from equation 2.4.23 with the result from equation 2.4.4, which 407 represents Heaviside's induction law, shows that under the stated conditions of a distorti-408 on-free magnetic flux density and a distortion-free volume, that same induction law increases 409 by a factor of 2. It needs to be expanded if the assumptions made in deriving equation 2.4.23 410 hold. That is why the formulation for the time-dependent magnetic moment  $\vec{m}_{(t)}$  must now 411 be expanded by this factor; it must be reformulated.

### 2.5 THE REFORMULATION OF THE MAGNETIC MOMENT

The fact explained in Chapter 2.4 means that the formulation for the time-dependent magne-

413 414

415

416 tic moment  $\vec{\mathbf{m}}_{(i)}$  from equation 2.4.3 is also influenced. 417  $\vec{\mathbf{m}}_{(t)} = \left(\frac{\left(-\frac{\delta \vec{B}}{\delta t} \cdot \vec{A}\right)}{R}\right) \cdot \vec{A}$ 418 (2.4.3)419 In equation 2.4.3, the formulation from equation 2.4.4 can now be replaced by the 420 formulation from equation 2.4.23. This turns equation 2.4.3 into equation 2.5.1. 421 422  $\vec{\mathbf{m}}_{(t)} = \left(\frac{(-2 \cdot \frac{dB}{dt} \cdot \vec{A})}{R}\right) \cdot \vec{A}$ 423 (2.5.1)424 This also results in an adjustment for equation 2.3.1. This is shown in equation 2.5.2. 425 426 427  $\vec{\mathbf{m}}_{(t)} = \mathbf{i}_{(t)} \cdot \vec{A}$ (2.3.1)428 429  $\vec{\mathbf{m}}_{(t)} = 2 \cdot \mathbf{i}_{(t)} \cdot \vec{A}$ 430 (2.5.2)431 The comparison between equation 2.3.1 and equation 2.5.2 shows why there is a difference of 432 433 a factor of 2 between the measured value and the calculation for the time-dependent magnetic 434 moment in the experiments described in chapter 2.1. 435 436 3. Discussion 437 438 1. Apart from the situation presented in this paper, are there other possibilities of calculation 439 440 errors in the Einstein de Haas experiment with regard to factor 2 in equation 2.4.23? 441 2. What impact does the situation presented in this paper have on the Landé G factor? 442 443 3. What effects does the facts presented in this paper have on the gyromagnetic factor g? 444

446 4. What effects does the facts presented in this paper have on the physical area of quantum447 mechanics? Theories regarding spin and intrinsic angular momentum of the electron may be448 affected.

449

450 5. What effects does the facts presented in this paper have on the physical subfield of451 electrodynamics? The "Maxwell equations" and the Lorenz force are affected here.

452

453 6. What effects does the facts presented in this paper have on the physical subfield of solid454 state physics? Ferromagnetism and superconductivity can be affected.

455

456 7. Are there other areas of physics that are influenced by the facts presented in this paper and457 if so, which ones and how?

- 458
- 459
- 460
- 461

# **4. CONCLUSION**

Under the mathematical requirement from equation 2.2.7, based on the magnetic flux density  $\vec{B}$ , to be exact  $(Sp)(grad \vec{B}) = div(\vec{B})$ , the physical requirement based on the assumption that the divergence of the magnetic flux density  $\vec{B}$  is fundamentally assigned the value 0 (  $div(\vec{B}) = 0$  ) is only valid under the assumption, that the value of the trace of the magnetic flux density gradient is also 0 (  $(Sp)(grad \vec{B}) = 0$  ). However, since the trace of the gradient of the magnetic flux density  $(Sp)(grad \vec{B}) = 0$  ). However, since the magnetic flux density  $div(\vec{B})$  contain the elements that, in combination with the velocity vector

469 
$$\vec{v}$$
, describe the expression  $-\frac{\delta \vec{B}}{\delta t}$ , to be exact  $\frac{\delta B_x}{\delta x}$ ,  $\frac{\delta B_y}{\delta y}$  and  $\frac{\delta B_z}{\delta z}$ , these two

470 expressions are mathematically inseparable from each other. This leads to either the physical 471 concept of the magnetic field having to be reinterpreted or the assumption that the divergence 472 of the magnetic flux density basically has the value 0 (  $\operatorname{div}(\vec{B}) = 0$  ) is wrong. This was 473 sufficiently explained in the paper "The reinterpretation of the 'Maxwell equations'[1]". For 474 the Einstein de Haas experiment, the consequence is that equation 2.3.1 for the time-depen-475 dent magnetic moment  $\vec{m}_{(t)}$  must be expanded by a factor of 2. This results in a new equa-476 tion for the time-dependent magnetic moment  $\vec{m}_{(t)}$ , to be exact equation 2.5.2. Other areas

477	of physics are also affected, including quantum mechanics. The task now is to identify these
478	sub-areas and then correct them based on the facts presented here.
479	Due to the discrepancy between the measured value and the calculated value, the Einstein de
480	Haas experiment can also be assumed to be experimental evidence that the facts from the ela-
481	boration "The reinterpretation of the 'Maxwell equations'[1]" are correct.
482	
483	
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