EUV Lithography Design Concepts using Diffraction Optics

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Abstract:

This presentation outlines design concepts for maskless and mask-projection (holographic) EUV lithography at wavelength 13.5 or 6.7 nm.

Presentation Outline

- 1. Review maskless EUVL design concept
- 2. Simplified chromatic correction with diffractive collection mirror
- 3. Extension from maskless to mask-projection, "holographic" EUVL

See slide notes, page 21.



Geometric Aberration Compensation

Without aberration compensation:

With aberration compensation:



Lens zone pattern (at outermost field position)



Phase aberration over exit pupil

uncorrected image phase error at λ =13.5nm (1.0-wave RMS, 3.9-wave P-V)

corrected image phase error at λ =13.5nm (0-wave RMS, P-V)





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Diffractive Projection Optics



Diffractive Mirror Fabrication

Deposit ~70 Mo/Si bilayers for λ =13.5nm (or ~200 B/La for 6.7nm):



Form a quadratic bowl, ~24 bilayers center depth, via IBF processing:



Chromatic aberration over exit pupil



Chromatic aberration over exit pupil



Holographic mask-projection EUV lithography

Maskless, spot-scanning



Mask-projection (field stepper)





Reflection mask



Holographic lithography



Apodized field stitching

mask geometry:



Mask layout options

16 fields per mask:



Wafer tiling pattern



Summary/Conclusions

Maskless EUVL can be implemented using conventional binary, zone-plate EUV lens technology, and conventional IBF mirror processing for achromatization.

If phase-Fresnel EUV lenses are feasible, maskless efficiency could be doubled, and holographic mask-projection EUVL (with much higher throughput) might also be possible.

Benefits of holographic EUVL (vs conventional mask imaging) include:

- High dose and/or throughput, especially for sparse patterns
- Full aberration correction with simple and efficient projection optics
- Minimal defect sensitivity
- Minimal 3-D mask effects

Maskless and/or holographic EUVL could work for Blue-X (λ =6.7nm).

Selected References

Maskless EUVL

Maskless EUV lithography, an alternative to e-beam

https://doi.org/10.1117/1.JMM.18.4.043501 https://www.euvlitho.com/2019/P22.pdf

EUV Microlenses

Fabrication and performance of transmission engineered molybdenum-rich phase structures in the EUV regime

https://doi.org/10.1117/12.2281487

X-ray Fresnel Zone Plate (NTT product specs)

https://www.ntt-at.com/product/x-ray_FZP/

Blazed X-ray Optics

https://www.psi.ch/en/lmn/blazed-x-ray-optics https://www.psi.ch/en/lmn/double-sided-zone-plates

IBF-processed EUV mirror coatings

Homogenized ion milling over the whole area of EUV spherical multilayer mirrors for reflection phase error correction https://iopscience.iop.org/article/10.1088/1742-6596/425/15/152009/pdf

High-efficiency spectral purity filter for EUV lithography

US Patent 7,050,237 <u>https://patents.google.com/patent/US7050237B2/en</u>

Ion Beam Figuring (Buhler)

https://www.buhlergroup.com/content/buhlergroup/global/en/products/leybold_optics_ibfseriesionbeamfiguringmachine.html

Holographic/Phase-shift/Interference EUVL

Holographic mask for lithographic apparatus and device manufacturing method

US Patent 7,499,149 https://patents.google.com/patent/US7499149B2/en

Sub-Wavelength Holographic Lithography

https://nanotech-swhl.com/downloads.html

Holographic masks for computational proximity lithography with EUV radiation

https://doi.org/10.1117/12.2502879 https://www.euvlitho.com/2019/S34.pdf

Ultrahigh efficiency EUV contact-hole printing with chromeless phase shift mask

https://doi.org/10.1117/12.2243321 https://doi.org/10.1117/12.2260412

EUV Interference Lithography

https://www.psi.ch/en/lmn/euv-interference-lithography

EUVL Aberration Correction

Single spherical mirror optic for extreme ultraviolet lithography enabled by inverse lithography technology https://doi.org/10.1364/OE.22.025027

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- This is a continuation of my presentation on maskless EUVL at the 2019 Workshop and my JM³ paper. (See References, page 20.)

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- An LPP EUV source (e.g. Adlyte) can supply multiple scan modules.
- ~2 million microlenses focus EUV illumination through individual focal points, 0.09-NA convergence cones.
- The point array is imaged at 6X reduction onto the wafer at 0.55 NA (same NA as the EXE 5000).
- The wafer is raster-scanned while the points are modulated to sythesize a digital exposure image.
- The microlenses are supported by a microchannel plate with conical holes (TSV's) for beam transmission.
- MEMS shutters can be placed at the microlens foci (~1-micron travel range) to modulate each point.
- Alternatively, for printing periodic patterns (e.g. contact holes, DRAM cell arrays, etc.), a spatial light modulator might not be needed. Just modulate the source; all lens channels print identical patterns.
- The microlenses are binary-optic zone-plate elements, much simpler than what I proposed in 2019.
- The lenses are not achromatic; instead the system uses a diffractive M2 mirror to correct the chromatic aberration.

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- The system only needs two EUV projection mirrors because the microlenses can be designed to correct projection system aberrations.
- Zero-aberration imaging (at wavelength 13.5 nm) over wide image field, high NA.

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- Zone-plate lens illustration (at edge of object field), showing elliptically distorted phase zones to correct aberration.
- The black ellipse is the obscuration zone (distorted by aberration).
- Mo phase-shift rings (~85-nm thick) on Si substrate (50-100 nm), for wavelength 13.5-nm (or ~200 nm La on 100-200nm B4C for 6.7 nm)

- Optical phase error over exit pupil, without and with aberration correction.
- u2 and u3 are ray direction cosines at the image, for an image point at the edge of the field.
- Without correction: 1-wave RMS (could be reduced to <0.2-wave RMS, but the phase slope would be very steep, more difficult to correct)
- The radial gradient of the phase error is zero on the pupil boundary, enables aberration correction without lens distortion or increased zone density.
- With correction: Zero phase error at 13.5 nm (but the lenses will exhibit chromatic aberration at other wavelengths).
- Lens zone widths control pupil illumination profile.

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- Achromatic microlens system (left, proposed in 2019), simpler singlet lens (right, current design).
- The achromatic system requires:
 - 2 lenses in series, aligned on opposite sides of a microchannel plate
 - phase-Fresnel lenses (not easy to manufacture)
 - embedded MEMS shutters and data paths, if a spatial light modulator us used
- The singlet lenses can be simple binary-optic zone plates single-layer litho processing, minimum half-pitch 75 nm (similar to lenses CXRO has been making for ~20 years, but needs to be scaled up to large arrays, ~2 million lenses).
- A binary-optic lens will have half the efficiency of a phase-Fresnel lens, but the beam goes through only one lens so efficiency is similar to the achromatic doublet.
- A binary-optic lens will generate a lot of optical scatter/flare in extraneous diffraction orders, but not a problem because the beam can be spatially filtered at the focal point.
- A singlet lens will exhibit significant chromatic aberration, but the projection system can correct the chromatic aberration.

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- Chromatic-correction diffraction structure on mirror M2
- Phase structure similar to microlens (~24 annular zones), but scaled up from 15-micron to 600-mm aperture.

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- Fabrication process for diffractive M2 mirror (can work for wavelength 13.5 nm or 6.7 nm)
- Apply Ion Beam Figuring (IBF) to carve out a quadratic bowl in an EUV multilayer mirror, center depth ~24 bilayers.
- IBF is a well established process for optics fabrication, has been used to process EUV mirror coatings (see References).
- The reflection layers act as a volume Bragg-diffraction grating. Efficiency in the first diffraction order is very similar to a standard EUV mirror, but the layer tilt relative to the boundary surface results in some chromatic aberration, which nullifies the microlens chromatic aberration.

- Chromatic performance (phase aberration over exit pupil) without M2 correction, for 3 wavelengths: 13.5 nm (center) and 13.5+/-0.15 nm (right, left).
- 0.084-wave RMS (i.e. 1.1 nm @ 13.5-nm wavelength) chromatic focus change at the high/low wavelengths.

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- Chromatic performance with IBF-processed M2 mirror: 0.0067-wave RMS (i.e., 0.090-nm) at edge of image field (worst-case, less near center of the field)
- The residual phase error is mainly due to mirror axial symmetry it can only correct axially symmetric chromatic phase errors, but the peripheral microlenses are slightly asymmetric due to geometric aberration correction.
- This is for wavelength 13.5 nm. At 6.7 nm the residual chromatic phase error would be doubled (to 0.013 wave RMS).
- Reducing the projection optics scale by half (from 600-mm aperture to 300-mm aperture) would reduce the phase error by 2X, so similar performance at wavelength 6.7 nm should be achievable with a downsized projection system.

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- Next steps for future development:
- Replace the binary zone-plate lenses with phase-Fresnel lenses for doubled optical efficiency.
- If the phase-Fresnel lens quality is good enough (negligible scatter/flare), then the focal-plane spatial filter is not required and the filter and microchannel plate can be eliminated, leaving a free-standing thin film ("patterned pellicle").
- Without the microchannel plate, any kind of diffraction pattern can be used (not just microlens patterns); can be used for mask-projection (not maskless) EUVL with transmission mask.
- "Holographic" EUVL: Mask is displaced from focal plane, is not imaged directly onto wafer.
- Microlens-type mask structures can be used for isolated point patterns, but with static imaging, not scanning very high dose for isolated features (e.g. line cuts).
- Grating-type mask structures can be used to print dense line/space patterns via interference lithography; relatively high dose because there is no absorber.

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- Mask design can be simplified by putting a zero-order stop in the projection system (in the obscuration zone, supported by spider struts or pellicle).
- Dark-field imaging: To leave an area on the wafer unexposed, just don't pattern the mask. No need for zero-order extinction.

- Another design variant: Make the zero-order stop a mirror for directing illimitation onto a reflection mask.
- Normal incidence, minimal 3-D effects.
- Analogous to Lasertec actinic mask inspection system, which also has an axial fold mirror in the illumination optics.
- Use 45°-incidence fold mirror for polarized illumination (could be useful for very high-NA interference lithography).

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- Holographic reflection mask example: grating structure for printing dense line/space patterns at 8-nm half-pitch.
- Center region splits EUV illumination evenly into +1 and -1 orders for interference lithography.
- Side region generates only one first (+1 or -1) diffraction order; the other order is suppressed. Efficiency is matched to beam-splitter grating; lateral position controls phase matching.
- Zero order is no problem it is masked in the projection optics. 2nd and higher orders are outside the NA limit.

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- Field size is ~30 mm on mask, 5 mm on wafer.
- Large-field coverage via field stitching (similar to EXE 5000).
- Use overlapped exposure fields (e.g. hexagonal) and apodized illumination to avoid diffraction effects on the stitch lines.

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- Mask layout options: single exposure field per mask (cookie-size), or 16 fields on a more standard mask size.

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- Field tiling on waver: 64 exposure fields per standard die (26 mm by 33 mm).

- Re "Minimal defect sensitivity" for holographic EUVL: Mask defects are not in the focal plane, will be out of focus at the wafer.
- Re "Minimal 3-D mask effects":
 - Important for Blue-X (6.7-nm wavelength) reflection masks will require ~200 bilayers.
 - Transmission masks would probably have no significant 3-D effects.
 - Normal incidence illumination on reflection masks would minimize 3-D effects.
 - Holographic lithography might have sufficient degrees of freedom to nullify any 3-D effects.