Electronic data transmission at three times the speed of light and data rates of 2000 bits per second over long distances in buffer amplifier chains

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Abstract

During the experimental testing of basic assumptions in electrical engineering, it has become apparent that ultralow-frequency (ULF) voltage signals in coaxial cables with a length of only a few hundred meters propagate significantly faster than light. The starting point for this discovery was an experiment in which a two-channel oscilloscope was connected to a signal source via both a short and a long coaxial cable. It was observed that the delay between the two channels for short cables and low frequencies can be so small that the associated phase velocity exceeds the speed of light by one order of magnitude. To test whether the discovered effect can be exploited to transmit information over long distances, a cable was examined in which the signal was refreshed at regular distances by buffer amplifiers. The results show that such a setup is indeed suitable for transmitting wave packets at three times the speed of light and bit rates of approximately 2 kbit/s over arbitrary distances. The statement that information cannot propagate faster than light seems to be false and can no longer be sustained.

1. Introduction

In current information technology, hardly any speech or audio signals are transmitted as analog signal in the baseband, since this is accompanied by numerous disadvantages such as high sensitivity to noise and low information density. Even the transmission of information by means of electrical voltage is on the decline, since information can be transmitted much better optically over long distances.

In the past, however, the transmission of information via telephone cables played a key role in communications engineering, and there even arose a separate discipline dealing with the transmission properties of electrical cables. This sub-discipline of electrical engineering, known as the transmission line theory, is based on the telegrapher's equations [1, p. 307 et seq]. It is primarily concerned with the question of how signals propagate in transmission lines whose length is roughly the order of the wavelength of the transmitted signals or longer. However, ULF signals have wavelengths of 100 - 1000 kilometers, and it is obvious that transmission line theory may provide incorrect results for cables of short lengths.

It transpires that the transmission line theory does indeed fail for short cables and low frequencies. Nevertheless, it is rather astonishing that there is not a single experiment that measures the phase velocities of ULF signals in cables that are very short as compared with the transmitted wavelength. The author can only assume that this omission is related to the apparent lack of technological relevance, the dominance of the special theory of relativity, and the belief that someone else has already performed such measurements.

In fact, the question of how fast slowly oscillating electrical signals propagate is of great theoretical interest. If one permits the idea that the vacuum is a dielectric medium, the propagation velocity would be a simple material constant; at the same time, however, it would be unclear how fast the actual electrical force propagates. Some scientists have studied this question theoretically and experimentally by investigating how fast the electric force propagates in the three-dimensional space around moving charges in the near-field [2] [3].

As the authors of the cited articles already suspected, the actual electric force in the near field appears to propagate much faster than light. The present article demonstrates experimentally that this particularly applies to copper cables and opens up new technological possibilities.

2. Experimental setup

2.1. Hardware

The experiment is simple and can be easily reproduced. For the measurements, a PicoScope with AWG (arbitrary waveform generator), BNC connection cables and connectors, a Debian or Ubuntu Linux PC, several hundred meters of coaxial cable (RG6 PVC, 135 dB, characteristic impedance: 75 Ohm, 0.12 Ω/m , 50 pF/m), and software are needed, the source codes for which can be downloaded from Github [4]. The basic idea is to connect one input of the oscilloscope with a short cable and the other input with a long cable to the same signal source and measure the delay (Figure 1). It is important to note that the cable *must not be rolled up*, since the mutual inductance would almost completely inhibit the effect.

Since the PicoScope has an integrated signal generator (AWG), the oscilloscope itself can be used as a signal source for different frequencies. A further advantage of a PicoScope is that it can transfer the measurement data to a PC via USB (PicoScope 2204A: 1 MHz / PicoScope



Figure 1: Experimental setup: The long cable must not be rolled up!

3206D: up to 125 MHz). This enables the PC to store the recorded signals and perform an analysis. Since the Pico-Scope signal generator output has an internal resistance, it is recommended that a buffer amplifier (BA) be used directly behind the output and before the BNC T-adapter for longer cable lengths (Figure 2). For cables with a length of up to 300 m this is not necessary.



Figure 2: Used buffer amplifier

2.2. Software

For the experiment, software was developed that configures a PicoScope (PicoScope 2000 or 3000 Series with AWG) in such a way that it outputs a sine wave signal at the output of the function generator for a certain time, simultaneously samples both inputs with sample rates between 1 and 125 MHz, and transmits the data to the PC. The PC stores the received sample streams in a stereo WAVE file, which has the advantage that the recorded signals can be easily opened and analyzed using audio tools such as Audacity.

To determine the time delay between the two channels, the software has implemented two different methods. The figures 3 and 4 show the basic components of the signal processing algorithms. The software is available as a source code and can be freely downloaded from Github[4]. It is noted that the results documented below were obtained with a PicoScope 2204A, 65 s recording time, 1 MHz sampling rate and the method shown in Figure 3. Similar results were also obtained with other oscilloscopes, parameters, sample rates, with and without buffer amplifier, algorithms and even other cable types, such as single-core wire with a diameter of 0.5 mm without shielding. It can therefore be excluded with certainty that the observed much too high propagation velocities was caused by measurement or interpretation errors. The only crucial requirement for the occurrence of the effect seems to be to prevent the long cable or wire from influencing itself by mutual inductance.

3. Findings

3.1. Phase velocities

In the first stage of the experiment, phase velocities were determined as a function of frequency and conductor length. For this purpose, sine wave signals with frequencies of 1000, 1252, 1568, 1964, 2460, 3080, 3857, 4831, 6050, 7576, 9488, 11882, 14880, 18634, 23336, 29224, 36598, 45833, and 57397 Hz and cable lengths of 500, 300, 200, and 100 meters were examined. For each configuration, several measurements were performed and repeated at different times. Furthermore, the longer cable was sometimes connected with the first input of the oscilloscope and sometimes with the second. The measured delays τ are shown in Figure 5. Note that the error bars for the standard deviations are 20-times amplified.

The following functions for the signal delays were determined by curve fitting of the data:

$$\tau_{100m}(f) = 3.31 \cdot 10^{-8} \,\mathrm{s} + 2.80 \cdot 10^{-12} \,\mathrm{s}^2 f - 5.39 \cdot 10^{-17} \,\mathrm{s}^3 f^2 + 3.87 \cdot 10^{-22} \,\mathrm{s}^4 f^3, \tag{1}$$

$$\tau_{200m}(f) = 1.23 \cdot 10^{-7} \,\mathrm{s} + 1.12 \cdot 10^{-11} \,\mathrm{s}^2 f - 1.99 \cdot 10^{-16} \,\mathrm{s}^3 f^2 + 1.57 \cdot 10^{-21} \,\mathrm{s}^4 f^3$$
(2)

$$\tau_{300m}(f) = 2.76 \cdot 10^{-7} \,\mathrm{s} + 2.35 \cdot 10^{-11} \,\mathrm{s}^2 f - 3.85 \cdot 10^{-16} \,\mathrm{s}^3 f^2 + 3.22 \cdot 10^{-21} \,\mathrm{s}^4 f^3$$
(3)



Figure 3: Data evaluation algorithm based on filtering and subsequent convolution

$$\tau_{500m}(f) = 6.63 \cdot 10^{-7} \,\mathrm{s} + 1.49 \cdot 10^{-10} \,\mathrm{s}^2 f - 2.68 \cdot 10^{-14} \,\mathrm{s}^3 f^2 + 7.39 \cdot 10^{-18} \,\mathrm{s}^4 f^3 \tag{4}$$

Figure 6 shows the phase velocities

$$v_p(f) = \frac{\text{len}}{\tau_{\text{len}}(f)} \tag{5}$$

resulting from the measured delays in units of c. As can be seen, these are far beyond the speed of light for frequencies in the audio range ($f = 30 \dots 15000 \text{ Hz}$).

It should be noted that faster-than-light phase velocities with a cable length of 500 meters occur only at frequencies below approximately 5 kHz. For higher frequencies, the electromagnetic wave effects appear to increasingly dominate.

3.2. Signal delay of a music track as a function of cable length

To study whether extremely high phase velocities of ULF and VLF signals also lead to extremely high transmission speeds for general but band-limited signals, a soundtrack (classical music), namely "An End, Once and For All" from the computer game "Mass Effect 3", was transmitted via cables of different lengths. For this purpose, instead of the signal generator, the right loudspeaker output of a HiFi system was connected to the oscilloscope in two different ways: via a long coaxial cable and directly.

The cable lengths were varied, and the delays were determined. Furthermore, the input positions of the oscilloscope were differed again, i.e., the long cable was sometimes connected with input A and sometimes with input B. The measured delays showed little scattering and were reproducible and symmetrical with respect to the oscilloscope

input. The quality of the music was similar on both channels after transmission, with no audible difference. Table 1 summarizes the measurement results.

cable length	required time	velocity
100 m	39.6 ns	8.4 c
200 m	141.0 ns	4.7 c
300 m	319.2 ns	3.1 c
500 m	944.5 ns	1.8 c

Table 1: Measured propagation velocities of the audio signal

A visual check of the audio data showed that only the 500-meter cable showed a shift of approximately one sample between the channels. Since this corresponds to a time of 1000 ns at a sampling rate of 1 MHz, this is consistent with the results shown in table 1.

4. Increasing the signal range

4.1. Principle and measurement results

At this point, it was reasonable to assume that it may be possible to transmit ULF signals at velocities beyond the speed of light even over long distances *by refreshing the signal at regular distances*. To test this hypothesis, a 200meter coaxial cable was split in the middle, and a buffer amplifier (Figure 2) was inserted in between. Subsequently, as before, the signal delay was measured as a function of frequency. Figure 8 shows the results of the measurement.

By curve fitting the data, one obtains the function:

$$\hat{\tau}_{200m}(f) = 9.03 \cdot 10^{-8} \,\mathrm{s} + 5.59 \cdot 10^{-12} \,\mathrm{s}^2 f - 1.04 \cdot 10^{-16} \,\mathrm{s}^3 f^2 + 7.90 \cdot 10^{-22} \,\mathrm{s}^4 f^3.$$
(6)



Figure 4: Data evaluation algorithm with Fast Fourier Transform



Figure 5: Measured signal delays τ between the two channels as a function of cable length and signal frequency f (error bars are 20-times amplified).

As can be seen by calculating $\hat{\tau}_{200m}(f) - 2 \cdot \tau_{100m}(f)$, the buffer amplifier causes an almost frequency-independent delay of $\tau_{BA} = 24.1$ ns.

It is therefore obvious that, in principle, it is possible to transmit ULF signals over long distances at extremely high speeds. For example, if a buffer amplifier is used every 100 meters, the signal delay is:

$$\hat{\tau}_{100m}(f) = \tau_{100m}(f) + \tau_{BA} \tag{7}$$

per 100 meters of cable.

To further confirm this, a buffer amplifier chain consisting of four 100-meter coaxial cables and three buffer amplifiers was built and analyzed (Figure 7). Curve fitting of



Figure 6: Phase velocities v_p as a function of cable length and signal frequency f

the data resulted in:

$$\hat{\tau}_{400m}(f) = 2.14 \cdot 10^{-7} \,\mathrm{s} + 1.09 \cdot 10^{-11} \,\mathrm{s}^2 f - 1.92 \cdot 10^{-16} \,\mathrm{s}^3 f^2 + 1.43 \cdot 10^{-21} \,\mathrm{s}^4 f^3.$$
(8)

As one can see,

$$\hat{\tau}_{400m}(f) \approx 4 \cdot \tau_{100m}(f) + 3 \cdot \tau_{BA} \tag{9}$$

is a very good approximation of the measured values.

This shows that it is also possible to establish long transmission lines with extremely high phase velocities. In the case that a buffer amplifier is used every 100 meters, one obtains the de facto length-independent phase velocity:

$$\hat{v}_p(f) = \frac{100 \,\mathrm{m}}{\tau_{100m}(f) + \tau_{BA}}.$$
(10)



Figure 7: Buffer amplifier chain with 4 coaxial cable segments and 3 buffer amplifiers



Figure 8: Measured signal delay for the refreshed signal in comparison with non-refreshed transmissions (error bars are 20-times amplified).

Figure 9 shows this phase velocity as a function of frequency.

4.2. The transmission properties of a buffer amplifier chain

Section 4 has shown experimentally that it is possible to establish a transmission line in which signals with frequencies under 60 kHz propagate at several times the speed of light. If one connects 100-meter coaxial or twisted-pair cables with buffer amplifiers, one obtains a buffer amplifier chain of a freely configurable length. The fact that data can be transmitted over such a transmission line at bit rates of 2 kbit/s and a speed of approximately 3 c is discussed below.

The starting point is that a temporally localized signal is required for the transmission of a single bit, which ideally does not contain a DC component and only frequencies up to approximately 50 kHz. Such a signal is, for example (wave packet):

$$b(t) = e^{-2\pi^2 f_B^2 t^2} \cos\left(2\pi f_C t\right). \tag{11}$$

 f_C is hereby the carrier frequency and f_B a frequency that determines the bandwidth of the signal.

The spectrum of this signal can be obtained by calculat-



Figure 9: Phase velocity for a cable with signal-refresh every 100 meters

ing the Fourier transform:

$$\mathcal{F}\{b\}(f) = \int_{-\infty}^{+\infty} b(t) e^{i2\pi f t} dt$$

$$= \frac{1}{2} \left(g \left(f - f_C, f_B \right) + g \left(f + f_C, f_B \right) \right),$$
(12)

with g representing the Gaussian function:

$$g(x,\sigma) := \frac{1}{\sqrt{2\pi\sigma^2}} e^{-\frac{x^2}{2\sigma^2}}.$$
 (13)

The spectrum has the meaning of a distribution function of the frequencies in the signal. For this reason,

$$s(t,x) = \int_{-\infty}^{+\infty} \mathcal{F}\{b\}(f) \, e^{-i2\pi f \left(t - x/\hat{v}_p(|f|)\right)} \, \mathrm{d}f \qquad (14)$$

is the amplitude of the signal at the time *t* and the location *x*, since $e^{-i2\pi f(t-x/\hat{v}_p(|f|))}$ represents a propagating wave. For x = 0, as can be seen easily, one obtains the usual inverse Fourier transform, and the signal s(t, x = 0) corresponds to b(t). However, for x > 0, the signal is shifted. It is important to note that calculation of the absolute value in $\hat{v}_p(|f|)$ is necessary, since the integration also runs over negative frequencies, but the phase velocity (10) is only defined for $f \ge 0$.

For the signal (11), the integral (14) can be solved analytically by approximating the function $1/\hat{v}_p(|f|)$ at $f = f_C$ as a Taylor series of first-order, which corresponds to the tangent at this point. For $f_C = 30$ kHz, one obtains:

$$\frac{1}{\hat{v}_p(|f|)} \approx 8.48 \cdot 10^{-10} \frac{\text{s}}{\text{m}} + 6.11 \cdot 10^{-15} \frac{\text{s}^2}{\text{m}} |f|, \qquad (15)$$

which is a good approximation for a bandwidth parameter of $f_B = 5 \text{ kHz}$.



Figure 10: Signal propagation in an ideal ($v_p = c$ for all frequencies) transmission line (left) and in a buffer amplifier chain (right)

The solution of the integral (14) is, even by using the approximation (15), still too long to be written down here. For this reason, refer to figure 10: shown on the left side is how the signal s(t, x) for $f_C = 30$ kHz and $f_B = 5$ kHz propagates in an ideal transmission line with frequency-independent phase velocity $v_p(f) = c$; and shown on the right side for comparison is the voltage one would measure at a specific position at a certain time, if one were to use a buffer amplifier chain as a transmission line. As can be seen, in the buffer amplifier chain, the wave packet moves at a significantly higher velocity. At the same time, although dispersion occurs, the wave package remains intact. Moreover, it is noted that the higher width of the wave packet in the buffer amplifier chain is not primarily due to dispersion but the higher signal velocity and, therefore, the longer



Figure 11: Signal at a distance of 1000 km

wavelength. Figure 11 shows the voltage that one would measure at a distance of 1000 km.

As can be seen in Figure 10, wave packets transmitted at a time interval of approximately 0.5 ms would not interfere with each other and remain clearly distinguishable at a distance of 1000 km. This means that with the mentioned parameters for f_C and f_B , a bit rate of roughly 2000 bits per second is possible.

Since this bit rate is extremely small in comparison with current usual bit rates, the practical use of such a buffer amplifier chain is comparatively limited, especially since the effort for setup and operation would be relatively high. However, the small practical benefit is outweighed by the important theoretical insight that the speed of light is by no means the upper limit at which information can propagate.

5. Summary and final remarks

The article shows that the assumption of some scientists is correct that the electric force in the near field of an electrical charge propagates at a significantly higher velocity than light. To date, however, it was not clear to experts that this effect also occurs in copper lines and that it can have a range of several hundred meters. In addition, the scientific community was not aware that this effect can be used technologically to transmit information significantly faster than would be possible with light. How such a transmission line can be constructed was also explained and investigated; however, the consequences that the discovery will have on the theoretical foundations of electrical engineering were not discussed in this article.

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