

# On the change in electrical power caused by loading an electrical circuit with an impedance

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## Abstract

In this paper we apply the theory of two-ports to present and to proof two real-valued theorems and two complex-valued theorems on the difference in electrical power of an unloaded and a loaded circuit driven by a voltage source or a current source, respectively.

## 1 Theorems on real-valued impedances

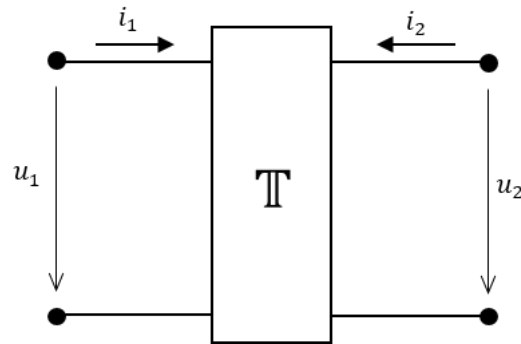


Figure 1

For given currents  $i_1$ ,  $i_2$  and a given two-port matrix

$$\mathbb{T} := \begin{bmatrix} a & c \\ c & b \end{bmatrix}$$

the voltages  $u_1$  and  $u_2$  can be determined from

$$\begin{bmatrix} u_1 \\ u_2 \end{bmatrix} = \mathbb{T} \cdot \begin{bmatrix} i_1 \\ i_2 \end{bmatrix}$$

We then have the following results:

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**Lemma**

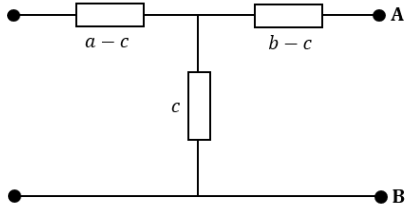


Figure 2

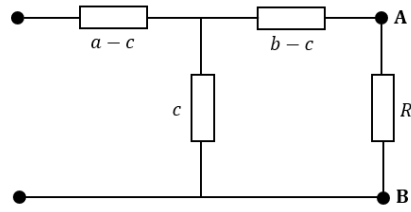


Figure 3

1. The equivalent resistance of the circuit shown in Figure 2 equals

$$R_e = a$$

2. The equivalent resistance of the circuit shown in Figure 3 loaded with resistor  $R$  equals

$$\tilde{R}_e = a - \frac{c^2}{b+R}$$

**Proof**

1.  $R_e = (a - c) + (c) = a \quad \square$

2.  $\tilde{R}_e = (a - c) + (c) \parallel ((b - c) + R) = (a - c) + \frac{c \cdot (b - c + R)}{c + (b - c + R)}$   
 $= a - \frac{c^2}{b + R} \quad \square$

From this lemma the following theorem can be derived:

**Theorem 1**

Let  $u$  be the source voltage of a circuit,  $u_o$  the open source voltage between the terminals A and B of the unloaded voltage source circuit and  $R_i$  the internal resistance of the unloaded voltage source circuit, respectively.

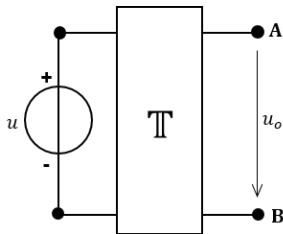


Figure 4

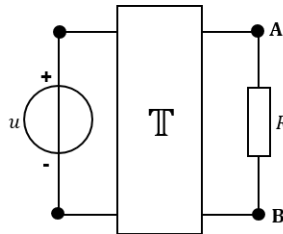


Figure 5

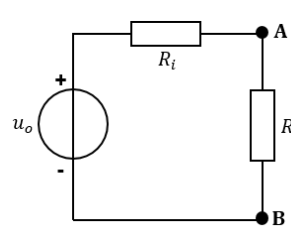


Figure 6

Let  $p$  be the electrical power of the unloaded circuit displayed in Figure 4. Further, let  $\tilde{p}$  be the electrical power of the circuit displayed in Figure 5 loaded with resistor  $R$ . Then

$$\tilde{p} - p = \frac{u_o^2}{R_i + R}$$

**Proof**

Let  $\mathbb{T}$  be the two-port matrix of the circuit

$$\mathbb{T} := \begin{bmatrix} a & c \\ c & b \end{bmatrix}$$

Using part (1) of the lemma

$$p = \frac{u^2}{R_e} = \frac{u^2}{a}$$

Using part (2) of the lemma

$$\tilde{p} = \frac{u^2}{\tilde{R}_e} = \frac{u^2}{a - \frac{c^2}{b + R}}$$

From the circuit displayed in Figure 4 it follows

$$u_o = \frac{c}{(a - c) + c} \cdot u = \frac{c}{a} \cdot u$$

and

$$R_i = (b - c) + c \parallel (a - c) = b - c + \frac{c \cdot (a - c)}{c + (a - c)} = \frac{a \cdot b - c^2}{a}$$

Then

$$\frac{u_o^2}{R_i + R} = \frac{\left(\frac{c}{a} \cdot u\right)^2}{\frac{a \cdot b - c^2}{a} + R} = \frac{c^2}{a \cdot (b + R) - c^2} \cdot \frac{u^2}{a} = \tilde{p} - p \quad \square$$

The theorem states that the change in electrical power between the loaded and the unloaded circuit equals the electrical power of the loaded Thévenin circuit:

$$P_{loaded} - P_{unloaded} = P_{Thévenin \ loaded}$$

From the previous lemma the following theorem can be derived:

**Theorem 2**

Let  $i$  be the current source of a circuit,  $u_o$  the open source voltage between the terminals A and B of the unloaded current source circuit and  $R_i$  the internal resistance of the unloaded current source circuit, respectively.

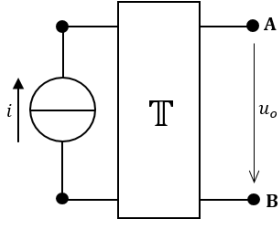


Figure 7

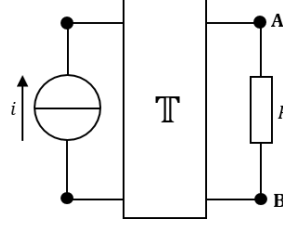


Figure 8

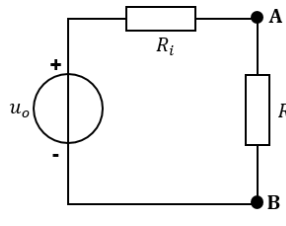


Figure 9

Let  $p$  be the electrical power of the unloaded circuit displayed in Figure 7. Further, let  $\tilde{p}$  be the electrical power of the circuit displayed in Figure 8 loaded with resistor  $R$ .

Then

$$p - \tilde{p} = \frac{u_o^2}{R_i + R}$$

**Proof**

Let  $\mathbb{T}$  be the two-port matrix of the circuit

$$\mathbb{T} := \begin{bmatrix} a & c \\ c & b \end{bmatrix}$$

Using part (1) of the lemma

$$p = i^2 \cdot R_e = i^2 \cdot a$$

Using part (2) of the lemma

$$\tilde{p} = i^2 \cdot \tilde{R}_e = i^2 \cdot \left( a - \frac{c^2}{b + R} \right)$$

From the circuit displayed in Figure 7 it follows that

$$u_o = i \cdot (c) = c \cdot i$$

and

$$R_i = (b - c) + (c) = b$$

Then, it holds that

$$\frac{u_o^2}{R_i + R} = \frac{(c \cdot i)^2}{b + R} = \frac{c^2}{b + R} \cdot i^2 = p - \tilde{p} \quad \square$$

Note that the expression  $p - \tilde{p}$  for the change in electrical power for a circuit connected across a current source equals  $-(\tilde{p} - p)$  where  $(\tilde{p} - p)$  expresses the change in electrical power for a voltage source.

The theorem states that the change in electrical power between the unloaded and the loaded circuit equals the electrical power of the loaded Thévenin circuit:

$$P_{\text{unloaded}} - P_{\text{loaded}} = P_{\text{Thévenin loaded}}$$

**Example 1**

Application of the derived theorems to the Wheatstone bridge/twin parallel voltage divider.

Given:  $R_1 = 10 \Omega$ ,  $R_2 = 40 \Omega$ ,  $R_3 = 20 \Omega$ ,  $R_4 = 30 \Omega$ .

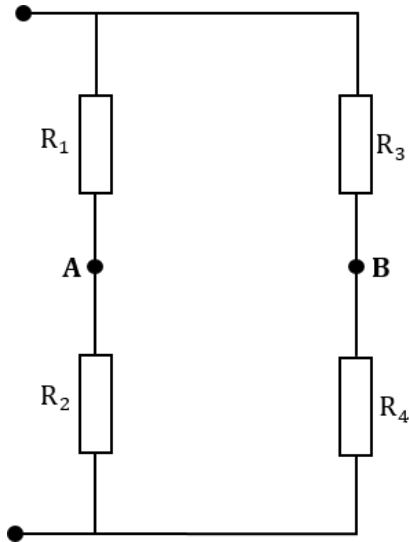


Figure 10

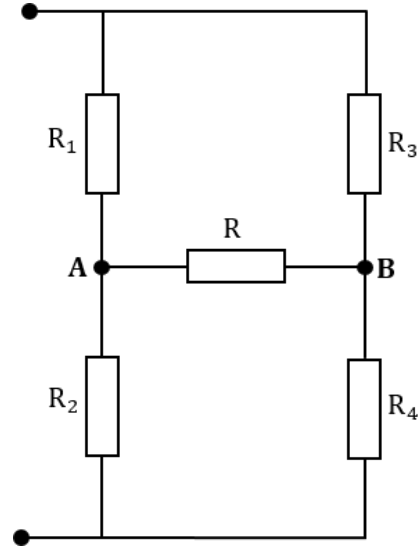


Figure 11

The two-port matrix of this circuit equals

$$\begin{aligned} \mathbb{T} &:= \begin{bmatrix} a & c \\ c & b \end{bmatrix} = \\ &= \frac{1}{R_1 + R_2 + R_3 + R_4} \cdot \begin{bmatrix} (R_1 + R_2) \cdot (R_3 + R_4) & R_2 \cdot R_3 - R_1 \cdot R_4 \\ R_2 \cdot R_3 - R_1 \cdot R_4 & (R_1 + R_3) \cdot (R_2 + R_4) \end{bmatrix} \\ &= \begin{bmatrix} 25 & 5 \\ 5 & 21 \end{bmatrix} \Omega \end{aligned}$$

The equivalent resistance of the unloaded circuit equals

$$R_e = a = 25 \Omega$$

The equivalent resistance of the circuit loaded with resistor  $R = 4 \Omega$  equals

$$\tilde{R}_e = a - \frac{c^2}{b + R} = 24 \Omega$$

Given the source voltage  $u = 600 \text{ V}$  of the circuit displayed in Figure 12

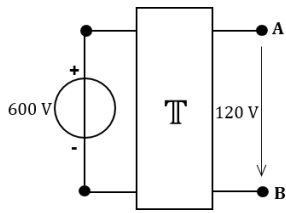


Figure 12

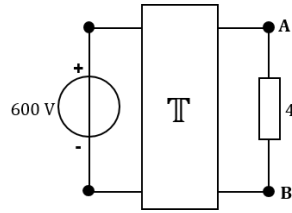


Figure 13

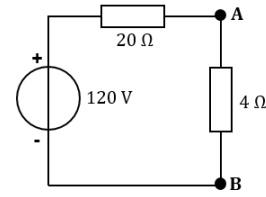


Figure 14

The electrical power of the unloaded circuit equals

$$p = \frac{u^2}{R_e} = 14400 \text{ W}$$

The electrical power of the circuit loaded with resistor  $R = 4 \Omega$  equals

$$\tilde{p} = \frac{u^2}{\tilde{R}_e} = 15000 \text{ W}$$

The open source voltage between the terminals A and B equals of the unloaded circuit equals

$$u_0 = \frac{c}{a} \cdot u = 120 \text{ V}$$

The internal resistance of the unloaded circuit

$$R_i = \frac{a \cdot b - c^2}{a} = 20 \Omega$$

The change in electrical power according to Theorem 1 amounts to

$$\tilde{p} - p = \frac{u_o^2}{R_i + R} = 600 \text{ W}$$

### Example 2

Given the source current  $i = 25 \text{ A}$  of the circuit displayed in Figure 15

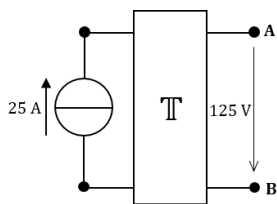


Figure 15

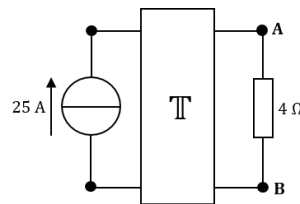


Figure 16

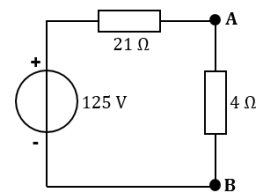


Figure 17

The electrical power of the unloaded circuit equals

$$p = i^2 \cdot R_e = 15625 \text{ W}$$

The electrical power of the circuit loaded with resistor  $R = 4 \Omega$  equals

$$\tilde{p} = i^2 \cdot \tilde{R}_e = 15000 \text{ W}$$

The open source voltage between the terminals A and B of the unloaded circuit amounts to

$$u_o = c \cdot i = 125 \text{ V}$$

The internal resistance of the unloaded circuit equals

$$R_i = b = 21 \Omega$$

The change in electrical power according to Theorem 2 is equal to

$$p - \tilde{p} = \frac{u_o^2}{R_i + R} = 625 \text{ W}$$

## 2 Theorems on complex-valued impedances

In the complex plane the power of an impedance can be expressed as

$$P := \frac{|U|^2}{Z^*} = |I|^2 \cdot Z$$

In the complex plane these expressions are no analytic functions of the complex source voltage  $U$  or the complex source current  $I$ . The electrical powers  $p$  and  $\tilde{p}$  are real-valued functions of the source voltage  $u$  or the source current  $i$  and the entries of the two-port matrix  $\mathbb{T}$ . The variables  $u$ ,  $i$  and the entries of the two-port matrix  $\mathbb{T}$  are real-valued. Yet, the domain of these variables can be extended to the complex plane, to obtain analytic continuations of the functions  $p$  and  $\tilde{p}$ . For this reason, the theorems stated and derived above, also apply to a complex valued source voltage  $U$  or a complex valued source current  $I$  and impedances.

### Theorem 3

Let  $U$  be the source voltage of a circuit and  $U_o$  being the open source voltage between the terminals A and B of the unloaded circuit. Let  $Z_i$  be the internal impedance of the unloaded circuit.

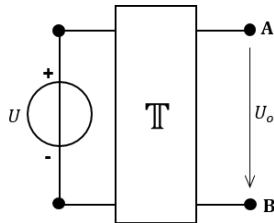


Figure 18

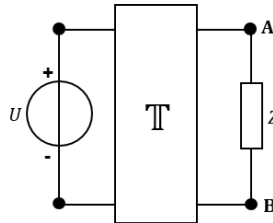


Figure 19

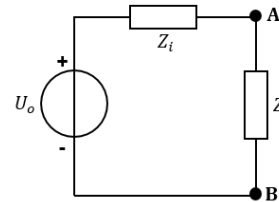


Figure 20

Let  $P$  the electrical power of the unloaded circuit displayed in Figure 18  
 Let  $\tilde{P}$  the electrical power of the circuit displayed in Figure 19 loaded with

impedance  $Z$ .

Then

$$\tilde{P} - P = \left( \frac{U_o^2}{Z_i + Z} \cdot \frac{U^*}{U} \right)^*$$

Remark: note that

$$\tilde{P} - P \neq \frac{|U_o|^2}{(Z_i + Z)^*}, \quad |\tilde{P} - P| = \left| \frac{|U_o|^2}{(Z_i + Z)^*} \right|$$

### Proof

According to Theorem 1

$$\tilde{p} - p = \frac{U_o^2}{Z_i + Z}$$

The proof proceeds by multiplying this identity with the factor  $U^*/U$  followed by conjugating the result:

$$\frac{U^*}{U} \cdot (\tilde{p} - p) = \frac{U^*}{U} \cdot \left( \frac{U^2}{\tilde{Z}_e} - \frac{U^2}{Z_e} \right) = \frac{U \cdot U^*}{\tilde{Z}_e} - \frac{U \cdot U^*}{Z_e} = \frac{|U|^2}{\tilde{Z}_e} - \frac{|U|^2}{Z_e} = \frac{U_o^2}{Z_i + Z} \cdot \frac{U^*}{U}$$

$$\left( \frac{|U|^2}{\tilde{Z}_e} - \frac{|U|^2}{Z_e} \right)^* = \frac{|U|^2}{\tilde{Z}_e^*} - \frac{|U|^2}{Z_e^*} = \tilde{P} - P = \left( \frac{U_o^2}{Z_i + Z} \cdot \frac{U^*}{U} \right)^* \quad \square$$

As remarked, the change in electrical power and the electrical power of the Thévenin circuit differ but are equal in magnitude.

### Theorem 4

Let  $I$  the current source of a circuit. Let  $U_o$  be the open source voltage between the terminals A and B of the unloaded circuit. Let  $Z_i$  be the internal impedance of the unloaded circuit.

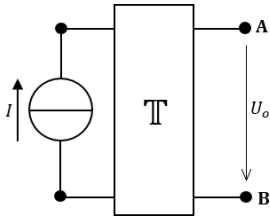


Figure 21

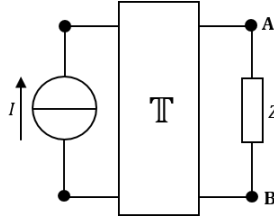


Figure 22

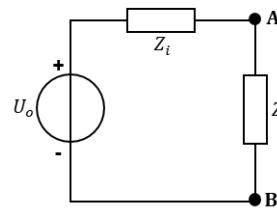


Figure 23

Let  $P$  be the electrical power of the unloaded circuit displayed in Figure 21 and  $\tilde{P}$  be the electrical power of the circuit displayed in Figure 22 loaded with resistor  $Z$ .

Then

$$P - \tilde{P} = \frac{U_o^2}{Z_i + Z} \cdot \frac{I^*}{I}$$



Remark. Note that

$$P - \tilde{P} \neq \frac{|U_o|^2}{(Z_i + Z)^*}, \quad |P - \tilde{P}| = \left| \frac{|U_o|^2}{(Z_i + Z)^*} \right|$$

**Proof**

According to Theorem 2

$$p - \tilde{p} = \frac{U_o^2}{Z_i + Z}$$

The proof proceeds by multiplying this identity with the factor  $I^*/I$ :

$$\begin{aligned} \frac{I^*}{I} \cdot (p - \tilde{p}) &= \frac{I^*}{I} \cdot (I^2 \cdot Z_e - I^2 \cdot \tilde{Z}_e) = I \cdot I^* \cdot Z_e - I \cdot I^* \cdot \tilde{Z}_e = \\ |I|^2 \cdot Z_e - |I|^2 \cdot \tilde{Z}_e &= P - \tilde{P} = \frac{U_o^2}{Z_i + Z} \cdot \frac{I^*}{I} \quad \square \end{aligned}$$

As has been remarked, the change in electrical power and the electrical power of the Thévenin circuit differ but are equal in magnitude.

**Example 3**

Given:  $Z_1 = -30j \Omega$ ,  $Z_2 = 10 \Omega$

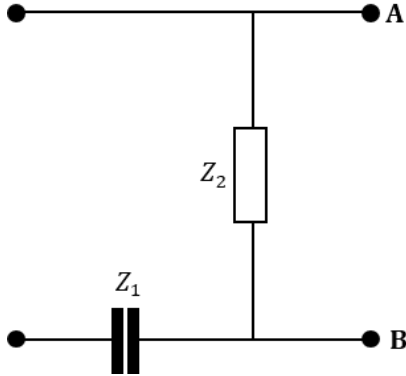


Figure 24

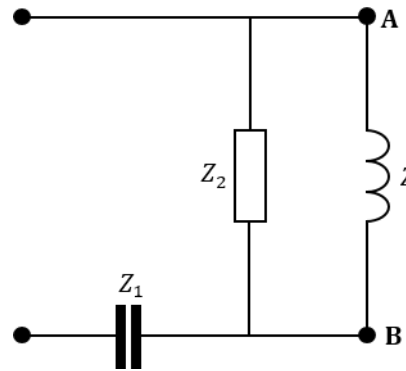


Figure 25

The two-port matrix of this circuit equals

$$\mathbb{T} := \begin{bmatrix} A & C \\ C & B \end{bmatrix} = \begin{bmatrix} Z_1 + Z_2 & Z_2 \\ Z_2 & Z_2 \end{bmatrix} = \begin{bmatrix} 10 - 30j & 10 \\ 10 & 10 \end{bmatrix} \Omega$$

The equivalent impedance of the unloaded circuit equals

$$Z_e = A = 10 - 30j \Omega$$

The equivalent impedance of the circuit loaded with impedance  $Z = 20j \Omega$  equals

$$\tilde{Z}_e = A - \frac{C^2}{B + Z} = 8 - 26j \Omega$$

Given the source voltage  $U = 740 + 370j$  V of the circuit displayed in Figure 26

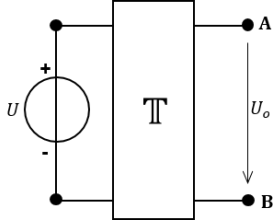


Figure 26

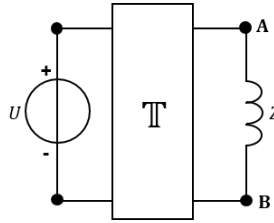


Figure 27

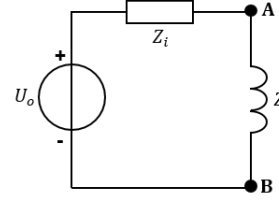


Figure 28

The electrical power of the unloaded circuit equals

$$P = \frac{|U|^2}{Z_e^*} = 6845 - 20535j \text{ VA}$$

The electrical power of the circuit loaded with impedance  $Z = 20j \Omega$  equals

$$\tilde{P} = \frac{|U|^2}{\tilde{Z}_e^*} = 7400 - 24050j \text{ VA}$$

The open source voltage between the terminals A and B of the unloaded circuit equals

$$U_o = \frac{C}{A} \cdot U = -37 + 259j \text{ V}$$

The internal impedance of the unloaded circuit equals

$$Z_i = \frac{A \cdot B - C^2}{A} = 9 - 3j \Omega$$

Change in electrical power according to Theorem 3

$$\tilde{P} - P = \left( \frac{U_o^2}{Z_i + Z} \cdot \frac{U^*}{U} \right)^* = 555 - 3515j \text{ VA}$$

Note that

$$\tilde{P} - P = 555 - 3515j \text{ VA} \neq \frac{|U_o|^2}{(Z_i + Z)^*} = 1665 + 3145j \text{ VA}$$

whereas

$$|\tilde{P} - P| = \left| \frac{|U_o|^2}{(Z_i + Z)^*} \right| = 185\sqrt{370} \text{ VA}$$

#### Example 4

Given

$$Z_1 = 15 \Omega, Z_2 = 30j \Omega, Z_3 = 40 \Omega$$

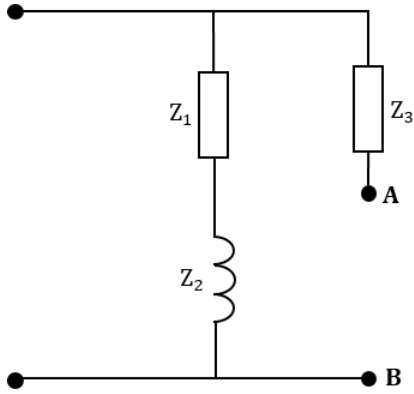


Figure 29: Circuit

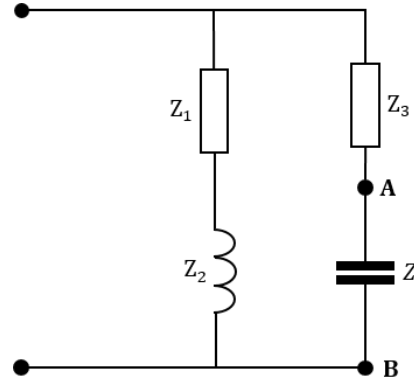


Figure 30: Circuit

The two-port matrix of this circuit equals

$$\mathbb{T} := \begin{bmatrix} A & C \\ C & B \end{bmatrix} = \begin{bmatrix} Z_1 + Z_2 & Z_1 + Z_2 \\ Z_1 + Z_2 & Z_1 + Z_2 + Z_3 \end{bmatrix} = \begin{bmatrix} 15 + 30j & 15 + 30j \\ 15 + 30j & 55 + 30j \end{bmatrix} \Omega$$

The equivalent impedance of the unloaded circuit equals

$$Z_e = A = 15 + 30j \Omega$$

The equivalent impedance of the circuit loaded with impedance  $Z = -20j \Omega$  equals

$$\tilde{Z}_e = A - \frac{C^2}{B + Z} = 24 + 12j \Omega$$

Given the source current  $I = 100 - 75j \text{ A}$  of the circuit displayed in Figure 31

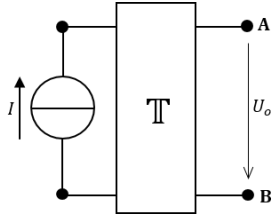


Figure 31

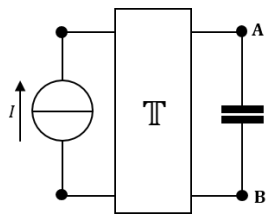


Figure 32

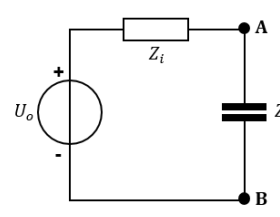


Figure 33

The electrical power of the unloaded circuit equals

$$P = |I|^2 \cdot Z_e = 234375 + 468750j \text{ VA}$$

The electrical power of the circuit loaded with impedance  $Z = -20j \Omega$  equals

$$\tilde{P} = |I|^2 \cdot \tilde{Z}_e = 375000 + 187500j \text{ VA}$$

The open source voltage between the terminals A and B of the unloaded circuit equals

$$U_o = C \cdot I = 3750 + 1875j \text{ VA}$$

The internal impedance of the unloaded circuit equals

$$Z_i = B = 55 + 30j \Omega$$

Change in electrical power according to Theorem 4

$$P - \tilde{P} = \frac{U_o^2}{Z_i + Z} \cdot \frac{I^*}{I} = -140625 + 281250j \text{ VA}$$

Note that

$$P - \tilde{P} = -140625 + 281250j \text{ VA} \neq \frac{|U_o|^2}{(Z_i + Z)^*} = 309375 + 56250j \text{ VA}$$

whereas

$$\left| P - \tilde{P} \right| = \left| \frac{|U_o|^2}{(Z_i + Z)^*} \right| = 140625\sqrt{5} \text{ VA}$$

### 3 Acknowledgement

The authors acknowledge the support of Ad Klein and of the Department of Engineering of Zuyd University of Applied Sciences.